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## EXHIBIT G Traffic Impact Study

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November 2022

## DAVISON INVESTORS DEVELOPMENT

2021

March

## TRAFFIC IMPACT ANALYSIS

ALONG COUNTY LINE ROAD/DAVISON ROAD IN CHARLESTON COUNTY, SOUTH CAROLINA



## DAVISON INVESTORS DEVELOPMENT

TRAFFIC IMPACT ANALYSIS

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March 2021

## TABLE OF CONTENTS

EXECUTIVE SUMMARY .....
1.0 INTRODUCTION ..... 1.1
1.1 PROJECT BACKGROUND ..... 1.1
1.2 EXISTING ROADWAY CONDITIONS ..... 1.1
2.0 DRIVEWAY SPACING REVIEW ..... 2.1
3.0 PROJECT TRAFFIC ..... 3.1
3.1 PROPOSED LAND USES ..... 3.1
3.2 TRIP GENERATION ESTIMATES ..... 3.1
3.3 TRIP DISTRIBUTION \& ASSIGNMENT ..... 3.1
4.0 TRAFFIC VOLUME DEVELOPMENT ..... 4.1
4.1 EXISTING TRAFFIC VOLUMES ..... 4.1
4.2 FUTURE TRAFFIC PROJECTIONS ..... 4.1
5.0 TRAFFIC IMPACT ANALYSIS ..... 5.1
5.1 TURN LANE ANALYSIS ..... 5.1
5.1.1 Right-Turn Lanes ..... 5.1
5.1.2 Left-Turn Lanes ..... 5.2
5.2 INTERSECTION LOS ANALYSIS ..... 5.3
6.0 SUMMARY OF FINDINGS AND RECOMMENDATIONS ..... 6.1
LIST OF TABLES
Table 2.1 - Minimum Driveway Spacing* ..... 2.1
Table 3.1 - Trip Generation Estimates ..... 3.1
Table 5.1 - Right-Turn Lane Criteria Warrants ..... 5.1
Table 5.2 - Left-Turn Lane Criteria Warrants ..... 5.2
Table 5.3 - HCM 2010 Intersection LOS Criteria ..... 5.3
Table 5.4 - Peak Hour Intersection Analysis Results ..... 5.4
LIST OF EXHIBIITS
Exhibit 1.1 - Davison Investors Development Location Map ..... 1.2
Exhibit 1.2 - Davison Investors Development Site Plan ..... 1.3
Exhibit 3.1 - Project Traffic Distribution and Assignment ..... 3.2
Exhibit 3.2 - AM and PM Peak Hour Project Traffic Volumes ..... 3.3
Exhibit 4.1-2020 Existing Peak Hour Traffic Volumes ..... 4.2
Exhibit 4.2 - Vested Traffic Volumes from the Nearby Poplar Grove Development ..... 4.3
Exhibit 4.3 - 2025 No Build Peak Hour Traffic Volumes ..... 4.4
Exhibit 4.4 - 2025 Build Peak Hour Traffic Volumes ..... 4.5
Exhibit 5.1-2025 No Build and Build Improved Level of Service Results ..... 5.5
LIST OF APPENDICES
Appendix A Trip Generation Worksheets Appendix B Traffic Volume Data Appendix C Traffic Volume Development Worksheets Appendix D Analysis Worksheets: 2020 Existing Conditions Appendix E Analysis Worksheets: 2025 No Build Conditions Appendix F Analysis Worksheets: 2025 Build Conditions Appendix G Analysis Worksheets: 2025 Build Conditions w/ Recommended Improvements Appendix H Turn Lane Analysis Worksheets

## EXECUTIVE SUMMARY

A traffic impact analysis was conducted for the proposed Davison Investors development in accordance with SCDOT and Charleston County guidelines.

The proposed Davison Investors development is located west of Davison Road and south of County Line Road in Charleston County, South Carolina and will consist of up to 390 singlefamily detached homes and 110 multifamily housing units (low-rise). While the development will be marketed primarily to active retirees, the trip generation potential for single-family detached homes and multifamily housing was used in an effort to be conservative.

Access to the development will be provided through up to five (5) proposed full access driveway(s) along the western/ southern side of Davison Road/County Line Road, all of which meet the SCDOT spacing requirements.

Therefore, the extent of the roadway network analyzed consisted of the five project driveway intersections as well as the signalized intersection of Davison Road \& US 17/Savannah Highway.

According to the current development plan, based on the turn lane criteria in SCDOT's Roadway Design Manual, exclusive westbound/northbound left-turn lanes along County Line Road/Davison Road are recommended at Project Driveways \#1, \#2, \#3, and \#4 prior to full buildout of the development. However, as the development is built out and/or the development plan changes, a detailed, phased traffic study may be performed in the future to determine the precise timing and threshold of development triggering the need for turn lanes.

The results of the intersection analysis indicate that the study intersections (including the intersection of US 17/Savannah Highway \& Davison Road) currently operate and are expected to continue to operate at an acceptable LOS with full build out of the proposed Davison Investors development, with only one exception at one of the project driveways:

The intersection of Davison Road \& Ten Shillings Way/Project Driveway \#1 is anticipated to experience undesirable delay in the PM peak hour of the 2025 Build Conditions. However, this projected delay is likely due to the conservative nature of the HCM 2010 unsignalized methodology and is not an uncommon condition for two-way stop control during the peak hours of the day. Therefore, no improvements to mitigate this delay are recommended.

### 1.0 INTRODUCTION

## $1.1 \quad$ PROJECT BACKGROUND

The purpose of this report is to document the procedures and findings of a traffic impact analysis for the proposed Davison Investors development in accordance with SCDOT and Charleston County guidelines. The proposed Davison Investors development is located west of Davison Road and south of County Line Road in Charleston County, South Carolina, as shown in Exhibit 1.1, and will consist of the following land uses, with anticipated completion in 2025:

* up to 390 Single-Family Detached Housing Units; and
* up to 110 Multifamily Housing (Low-Rise) Units.

Access to the development will be provided through up to five (5) proposed full access driveway(s) along the western/southern side of Davison Road/County Line Road, as shown in the site plan in Exhibit 1.2.

Project Driveway \#1 is proposed to align opposite of Ten Shillings Way; Project Driveway \#2 is proposed to be located between Ten Shillings Way and Bulow Landing Road; Project Driveway \#3 is proposed to align opposite of Bulow Landing Road; Project Driveway \#4 is proposed to align opposite of the existing Equestrian Center driveway; and Project Driveway \#5 is proposed to be located between Project Driveway \#4 and the existing Moberry Road/S-10-1447.

The traffic impact analysis considers the weekday AM peak hour (between 7:00 AM and 9:00 AM) and the weekday PM peak hour (between 4:00 PM and 6:00 PM) as the study time frames.

The extent of the existing roadway network to be studied consists of the 6 (six) intersections of:

1. Davison Road \& US 17/Savannah Highway;
2. Davison Road \& Ten Shillings Way/Project Driveway \#1
3. Davison Road \& Project Driveway \#2
4. Davison Road/County Line Road \& Bulow Landing Road/Project Driveway \#3;
5. County Line Road \& Equestrian Center Driveway/Project Driveway \#4; and
6. County Line Road \& Project Driveway \#5.

### 1.2 EXISTING ROADWAY CONDITIONS

County Line Road/Davison Road is a two-lane Major Collector that primarily serves residential and agricultural land uses. The posted speed limit is 45 mph and the average annual daily traffic (AADT) in 2019 was 3,800 vehicles/day. Based upon existing turning movement counts, the percentage of heavy vehicles along County Line Road/Davison Road is approximately $7 \%$.

US 17/Savannah Highway is a four-lane, divided Principal Arterial that primarily serves commercial and residential land uses. The posted speed limit is 55 mph and the average annual daily traffic (AADT) in 2019 was 34,900 vehicles/day. Based upon existing turning movement counts, the percentage of heavy vehicles along US 17/Savannah Highway is approximately $5 \%$.

Exhibit 1.1 - Davison Investors Development Location Map


Exhibit 1.2 - Davison Investors Development Site Plan


### 2.0 DRIVEWAY SPACING REVIEW

Access to the development will be provided through up to five (5) proposed full access driveway(s) along the western/southern side of Davison Road/County Line Road.

Project Driveway \#1 is proposed to align opposite of Ten Shillings Way; Project Driveway \#2 is proposed to be located between Ten Shillings Way and Bulow Landing Road; Project Driveway \#3 is proposed to align opposite of Bulow Landing Road; Project Driveway \#4 is proposed to align opposite of the existing Equestrian Center driveway; and Project Driveway \#5 is proposed to be located between Project Driveway \#4 and the existing Moberry Road/S-10-1447.

A review of the driveway spacing of the proposed driveways was completed based on information contained in SCDOT's Access \& Roadside Management Standards (ARMS) manual (2008), shown in the adapted Error! Reference source not found..

Table 2.1 - Minimum Driveway Spacing*

| Posted <br> Speed <br> Limit <br> $(\mathrm{mph})$ | AADT $\geq \mathbf{2 0 0 0}$; or <br> Driveways Generating <br> $>50$ Peak Hour Trips | AADT <2000 |
| :---: | :---: | :---: |
| 30 | 160 ft | 75 ft |
| 35 | 220 ft | 125 ft |
| 40 | 275 ft | 175 ft |
| 45 | 325 ft | 225 ft |
| $\geq 50$ | 400 ft | 275 ft |

*Figure 3-7 of Access \& Roadside Management Standards, 2008, SCDOT
Based upon the 45-mph speed limit and the driveway spacing criteria of ARMS, a minimum of 325 feet is required for full access along County Line Road/Davison Road.

Project Driveway \#1 is proposed to be aligned with the existing Ten Shillings Way, located approximately 550 feet south of the proposed Project Driveway \#2 and approximately 775 feet north of the next closest residential driveway to the south, both of which meet the spacing criteria.

Project Driveway \#2 is proposed to be located approximately 1,300 feet south of Bulow Landing Road and approximately 550 feet north of Ten Shillings Way, both of which meet the spacing criteria.

Project Driveway \#3 is proposed to be aligned with the existing Bulow Landing Road, located approximately 550 feet east of a proposed Poplar Grove Development driveway and approximately 1,800 feet north of Ten Shillings Way, both of which meet the spacing criteria.

Project Driveway \#4 is proposed to be aligned with the existing Equestrian Center driveway, located approximately 660 feet east of one proposed Poplar Grove development driveway and approximately 2,000 west of another proposed Poplar Grove development driveway, both of which meet the spacing criteria.

Project Driveway \#5 is proposed to be located approximately 1,300 feet east of the existing Moberry Road/S-10-1447 and approximately 1,400 feet west of a proposed Poplar Grove development driveway, both of which meet the spacing criteria.

## $3.0 \quad$ PROJECT TRAFFIC

## $3.1 \quad$ PROPOSED LAND USES

Project Traffic in this analysis is defined as the vehicle trips anticipated to be generated by the proposed Davison Investors development. These trips were distributed and assigned throughout the study roadway network.

The Davison Investors development is proposed to consist of the following land uses:

* up to 390 Single-Family Detached Housing Units; and
* up to110 Multifamily Housing (Low-Rise) Units.


### 3.2 TRIP GENERATION ESTIMATES

The trip generation potential for the development was estimated using information contained in ITE's Trip Generation Manual, 10 ${ }^{\text {th }}$ Edition (2017) reference. The estimates utilized the following land use codes:

* LUC 210 - Single Family Detached Housing; and
* LUC 220 - Multifamily Housing (Low-Rise).

Due to the nature of the proposed Davison Investors development, internal capture trips, pass-by trips, and multimodal reduction were not considered in the trip generation estimates. The trip generation estimates for the development are shown below in Table 3.1 and documented in Appendix A.

### 3.3 TRIP DISTRIBUTION \& ASSIGNMENT

New external traffic expected to be generated by the Davison Investors development was distributed and assigned to the roadway network based upon existing travel patterns in the area. The general distribution of project trips was assumed to be:

* 15\% to/from the west via County Line Road
* 70\% to/from the north via US 17/Savannah Highway
* $15 \%$ to/from the south via US 17/Savannah Highway

The assignment of new external project traffic anticipated to be generated by the Davison Investors development is illustrated in Exhibit 3.1 and the AM and PM peak hour project traffic volumes are illustrated in Exhibit 3.2.

Table 3.1 - Trip Generation Estimates

| Land Use | $\begin{aligned} & \text { ITE } \\ & \text { LUC } \end{aligned}$ | Scale | Daily | Weekday AM Peak Period |  | Weekday PM Peak Period |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Enter | Exit | Enter | Exit |
| Single Family Detached Housing | 210 | 390 Units | 3,638 | 71 | 211 | 236 | 139 |
| Multifamily Housing (Low-Rise) | 220 | 110 Units | 792 | 12 | 40 | 40 | 24 |
| New, External Trips |  |  | 4,430 | 83 | 251 | 276 | 163 |

Exhibit 3.1 - Project Traffic Distribution and Assignment


Exhibit 3.2 - AM and PM Peak Hour Project Traffic Volumes


### 4.0 TRAFFIC VOLUME DEVELOPMENT

### 4.1 EXISTING TRAFFIC VOLUMES

The traffic impact analysis considers the weekday AM peak hour (between 7:00 AM and 9:00 AM) and the weekday PM peak hour (between 4:00 PM and 6:00 PM) as the study time frames. The extent of the existing roadway network to be studied consists of the 2 (two) intersections of:

1. Davison Road \& US 17/Savannah Highway;
2. Davison Road \& Ten Shillings Way/Project Driveway \#1
3. Davison Road \& Project Driveway \#2
4. Davison Road/County Line Road \& Bulow Landing Road/Project Driveway \#3;
5. County Line Road \& Equestrian Center Driveway/Project Driveway \#4; and
6. County Line Road \& Project Driveway \#5.

Existing 2020 traffic volumes were collected at these study area intersections during the AM and PM peak periods listed above in August of 2019 and were not recollected in 2020 due to the impacts of the ongoing COVID-19 pandemic on traffic volumes. At the intersection of Davison Road \& Ten Shillings Way, existing traffic volumes in and out of Ten Shillings way were estimated based on a trip generation analysis of the number of homes using Ten Shillings Way for access (estimated to be 70 single-family-homes). At the intersection of County Line Road \& Equestrian Center Driveway, existing traffic volumes in and out of the Equestrian Center were estimated to be 10 vehicles in and 10 vehicles out in a peak hour based on the low trip generation potential of the existing center during typical weekday peak hours.

As noted in the subsequent section, traffic volumes in the study area are anticipated to grow at an annual rate of $2 \%$ per year. Therefore, the raw 2019 volumes were adjusted to 2020 Existing Conditions by applying a $2 \%$ growth rate for one year.

The raw traffic volume counts are provided in Appendix B and the 2020 existing AM and PM peak hour traffic volumes are illustrated in Exhibit 4.1 and documented in Appendix D.

### 4.2 FUTURE TRAFFIC PROJECTIONS

Future 2025 No Build traffic volumes were developed by adding background traffic growth and vested traffic to the collected Existing 2020 study area peak hour volumes. Background traffic growth is growth anticipated to occur in the study area regardless of the proposed Davison Investors development. Vested traffic is traffic anticipated to be generated by other known nearby developments expected to be completed prior to the Davison Investors development.

To develop an annual background growth rate for use in the analysis, historical count data from the last 15 years along US 17/Savannah Highway and Davison Road/County Line Road (SCDOT count stations \#109 and \#565) were reviewed. It was determined that the roadways have experienced a collected annual growth of $1.6 \%$. Therefore, to be conservative, a $2 \%$ annual growth rate was utilized to develop anticipated background traffic growth through the anticipated 2025 buildout year.

A separate project is currently proposed adjacent to the Davison Investors development. The Poplar Grove development, consisting of 450 Single-Family Homes, is located along County Line Road opposite of the Davison Investors Development in Dorchester County, South Carolina. The traffic volumes anticipated to be generated by this development were considered in the analysis as vested traffic, as illustrated in Exhibit 4.2.

2025 No Build AM and PM peak hour traffic volumes, illustrated in Exhibit 4.3, were developed by adding the background traffic growth (assuming 2\% annual growth of the existing traffic volumes) and the vested traffic from the nearby Poplar Grove development to the 2020 existing AM and PM peak hour traffic volumes.

2025 Build AM and PM peak hour traffic volumes, illustrated in Exhibit 4.4, were developed by adding the Davison Investors project traffic volumes (shown in Exhibit 3.1) to the 2025 No Build traffic volumes.

Volume development worksheets for each intersection are documented in Appendix C.

Exhibit 4.1-2020 Existing Peak Hour Traffic Volumes


Exhibit 4.2 - Vested Traffic Volumes from the Nearby Poplar Grove Development


Exhibit 4.3-2025 No Build Peak Hour Traffic Volumes


Exhibit 4.4-2025 Build Peak Hour Traffic Volumes


### 5.0 TRAFFIC IMPACT ANALYSIS

### 5.1 TURN LANE ANALYSIS

### 5.1.1 Right-Turn Lanes

An analysis was conducted to determine the potential need for exclusive right-turn lanes for ingress movements at the proposed project driveway(s). The need for exclusive rightturn lanes is based upon the criteria documented in Section 9.5.1.1 of SCDOT's Roadway Design Manual (2017), which consists of nine considerations, listed below:

1. At a free-flowing leg of any unsignalized intersection on a two-lane urban or rural highway which satisfies the criteria in Figure 9.5-A;
2. at a free-flowing leg of any unsignalized intersection on a high-speed ( 50 mph or greater), four-lane urban or rural highway which satisfies the criteria in Figure 9.5-B;
3. at the free-flowing leg of any unsignalized intersection on a six-lane urban or rural highway;
4. at any intersection where a capacity analysis determines a right-turn lane is necessary to meet the overall level-ofservice criteria;
5. as a general rule, at any signalized intersection where the projected right-turning volume is greater than 300 vehicles per hour and where there are greater than 300 vehicles per hour per lane on the mainline (A traffic analysis will be required if the turning volumes are greater than 300 vehicles per hour);
6. for uniformity of intersection design along the highway if other intersections have right-turn lanes;
7. at any intersection where the mainline is curved to the left and where the mainline curve requires superelevation;
8. at railroad crossings where the railroad is paralleled to the facility and is located close to the intersection and where a right-turn lane would be desirable to store queued vehicles avoiding interference with the movement of through traffic; or
9. at any intersection where the crash experience, existing traffic operations, sight distance restrictions (e.g., intersection beyond a crest vertical curve), or engineering judgement indicates a significant conflict related to right-turning vehicles;

Table 5.1 below details whether the previously mentioned criteria for exclusive right-turn lanes are satisfied for each driveway. An " $x$ " indicates that the criteria is not met; a " $\checkmark$ " indicates that it is met; and "N/A" indicates that the criteria is not applicable.

Table 5.1 - Right-Turn Lane Criteria Warrants

| Criteria | Project Driveway |  |  |  |  | Reference/Note |
| :---: | :---: | :---: | :---: | :---: | :---: | :--- |
|  | $\mathbf{1}$ | $\mathbf{2}$ | $\mathbf{3}$ | $\mathbf{4}$ | $\mathbf{5}$ |  |
|  | $x$ | $x$ | $x$ | $x$ | $x$ | Appendix H |
| 2 | N/A | N/A | N/A | N/A | N/A | Speed Limit < 45 mph |
| 3 | N/A | N/A | N/A | N/A | N/A | Not a six-lane highway |
| 4 | $x$ | $x$ | $x$ | $x$ | $x$ | Does not impact LOS |
| 5 | N/A | N/A | N/A | N/A | N/A | No signalized driveways |
| 6 | $x$ | $x$ | $x$ | $x$ | $x$ | No EB/SB right-turn lanes |
| 7 | N/A | N/A | N/A | N/A | N/A | No such curves |
| 8 | N/A | N/A | N/A | N/A | N/A | No railroad crossings |
| 9 | N/A | N/A | N/A | N/A | N/A | No known issues |

According to the current development plan, based on SCDOT's Roadway Design Manual considerations, exclusive eastbound/southbound right-turn lanes along County Line Road/Davison Road are not recommended at any of the project driveways (\#1, \#2, \#3, \#4, or \#5).

### 5.1.2 Left-Turn Lanes

An analysis was conducted to determine the potential need for exclusive left-turn lanes for ingress movements at the proposed project driveway(s). The need for exclusive left-turn lanes is based upon the criteria documented in Section 9.5.1.2 of SCDOT's Roadway Design Manual (2017), which consists of nine considerations, listed below:

1. At any unsignalized intersection on principal, high-speed rural highways with other arterials or collectors;
2. at any unsignalized intersection on a two-lane urban or rural highway that satisfies the criteria in Figures $9.5-\mathrm{C}$, 9.5-D, 9.5-E, 9.5-F, or 9.5-G;
3. at any intersection where a capacity analysis determines a left-turn lane is necessary to meet the level of service criteria;
4. at any signalized intersection where the left-turn volume is 300 vehicles per hour or more, conduct a traffic review to determine if dual left-turn lanes are required;
5. as a general rule, at any intersection where the leftturning volume is 100 vehicles per hour (for a single turn lane) or 300 vehicles per hour (for a dual turn lane);
6. at all entrances to major residential, commercial, and industrial developments;
7. at all median crossovers;
8. for uniformity of intersection design along the highway if other intersections have left-turn lanes (i.e., to satisfy driver expectancy); or
9. at any intersection where the crash experience, existing traffic operations, sight distance restrictions (e.g., intersection beyond a crest vertical curve), or engineering judgement indicates a significant conflict related to left-turning vehicles;

Table 5.2 below details whether the previously mentioned criteria for exclusive left-turn lanes are satisfied for each driveway. An " $x$ " indicates that the criteria is not met; a " $\checkmark$ " indicates that it is met; and "N/A" indicates that the criteria is not applicable.

Table 5.2 - Left-Turn Lane Criteria Warrants

| Criteria | Project Driveway |  |  |  |  | Reference/Note |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :--- | :---: |
|  | $\mathbf{1}$ | $\mathbf{2}$ | 3 | $\mathbf{4}$ | $\mathbf{5}$ |  |  |
| 1 | N/A | N/A | N/A | N/A | N/A | Not a high-speed arterial |  |
| 2 | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $x$ | Appendix H |  |
| 3 | $x$ | $x$ | $x$ | $x$ | $x$ | Does not impact LOS |  |
| 4 | N/A | N/A | N/A | N/A | N/A | No signalized driveways |  |
| 5 | $x$ | $x$ | $\checkmark$ | $x$ | $x$ | Exhibit 4.4 |  |
| 6 | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | Major residential develop. |  |
| 7 | N/A | N/A | N/A | N/A | N/A | No median |  |
| 8 | $x$ | $x$ | $x$ | $x$ | $x$ | No WB/NB left-turn lanes |  |
| 9 | N/A | N/A | N/A | N/A | N/A | No known issues |  |

According to the current development plan, based on the turn lane criteria in SCDOT's Roadway Design Manual, exclusive westbound/northbound left-turn lanes along County Line Road/Davison Road are recommended at Project Driveways \#1, \#2, \#3, and \#4 prior to full buildout of the development. However, as the development is built out, a detailed, phased traffic study may be performed in the future to determine the precise timing and threshold of development triggering the need for turn lanes.

Per the criteria documented in Section 5D-4 of SCDOT's Access and Roadside Management Standards (ARMS, 2008), it is recommended that, when installed, each of the exclusive left-turn lanes consist of a total of 380 feet, with 200 feet of storage and a 180 -foot taper.

Based on SCDOT's Roadway Design Manual considerations, an exclusive westbound left-turn lane is not recommended at Project Driveway \#5.

### 5.2 INTERSECTION LOS ANALYSIS

Using the existing and projected peak hour traffic volumes previously discussed, intersection analysis was conducted for the study and project driveway intersections considering 2020 Existing Conditions, 2025 No Build Conditions, and 2025 Build Conditions. The analysis was conducted using the Transportation Research Board's Highway Capacity Manual 2010 (HCM 2010) methodologies of the Synchro, Version 10 software for stop-controlled and signalized intersection analysis.

Intersection level of service (LOS) grades range from LOS A to LOS F, which are directly related to the level of control delay at the intersection and characterize the operational conditions of the intersection traffic flow. LOS A operations typically represent ideal, free-flow conditions where vehicles experience little to no delays, and LOS F operations typically represent poor, forced-flow (bumper-to-bumper) conditions with high vehicular delays, and are generally considered undesirable. Table 5.3 summarizes the HCM 2010 control delay thresholds associated with each LOS grade for unsignalized and signalized intersections.

Table 5.3 - HCM 2010 Intersection LOS Criteria

| LOS | Control Delay per Vehicle (s) <br> Unsignalized* | Signalized |
| :---: | :---: | :---: |
|  | $\leq 10$ | $\leq 10$ |
| B | $>10$ and $\leq 15$ | $>10$ and $\leq 20$ |
| C | $>15$ and $\leq 25$ | $>20$ and $\leq 35$ |
| D | $>25$ and $\leq 35$ | $>35$ and $\leq 55$ |
| E | $>35$ and $\leq 50$ | $>55$ and $\leq 80$ |
| F | $>50$ | $>80$ |

As part of the intersection analysis, SCDOT's default Synchro parameters were utilized.

The existing 2020 traffic counts' peak hour factors (PHF) were utilized in the analysis of existing conditions. Future-year 2025 conditions were analyzed utilizing existing PHF, but with a minimum PHF of 0.90 and maximum PHF of 0.95 considered.

The existing 2020 heavy vehicle percentages, as previously discussed, were utilized in the analysis, with a minimum percentage of $2 \%$ considered.

Existing lane geometry was utilized for the analysis of 2020 Existing Conditions and 2025 No Build Conditions. The 2025 Build Conditions were analyzed both with existing lane geometry and with any recommended improvements resulting from this impact analysis (including any recommended exclusive turn lanes per the results of Section 5.1) to illustrate their anticipated impact on traffic operations.

The results of the intersection analysis for existing and futureyear conditions for the weekday AM and PM peak hour time periods are summarized in Table 5.4.

For signalized intersections, the overall intersection LOS and delay results are evaluated for acceptable operation, while for two-way-stop-controlled (TWSC) intersections, the LOS and delay results are evaluated for the worst-case minor-street approaches only, per HCM 2010 methodologies for TWSC intersections.

Level of service A through $D$ is considered to be acceptable LOS, while LOS E and $F$ is considered to be undesirable.

Table 5.4 - Peak Hour Intersection Analysis Results

|  |  |  |  |  | LOS/Delay (seconds/vehicle) |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

As shown in Table 5.4 and illustrated below in Exhibit 5.1, the results of the analysis indicate that the study intersections currently operate and are expected to continue to operate at an acceptable LOS with the proposed Davison Investors development, with one exception:

The intersection of Davison Road \& Ten Shillings Way/Project Driveway \#1 is anticipated to experience undesirable delay in the PM peak hour of the 2025 Build Conditions, with or without the recommended turn lanes. However, this projected delay is likely due to the conservative nature of the HCM 2010 unsignalized methodology and is not an uncommon condition for two-way stop control during the peak hours of the day.

Worksheets documenting the intersection analyses are provided in Appendix D for 2020 Existing Conditions, Appendix E for 2025 No Build Conditions, Appendix F for 2025 Build Conditions, and in Appendix G for 2025 Build Conditions with recommended improvements (turn lanes).

Exhibit 5.1-2025 No Build and Build Improved Level of Service Results


### 6.0 SUMMARY OF FINDINGS AND RECOMMENDATIONS

A traffic impact analysis was conducted for the proposed Davison Investors development in accordance with SCDOT and Charleston County guidelines.

The proposed Davison Investors development is located west of Davison Road and south of County Line Road in Charleston County, South Carolina and will consist of up to 390 singlefamily detached homes and 110 multifamily housing units (low-rise). While the development will be marketed primarily to active retirees, the trip generation potential for single-family detached homes and multifamily housing was used in an effort to be conservative.

Access to the development will be provided through up to five (5) proposed full access driveway(s) along the western/ southern side of Davison Road/County Line Road, all of which meet the SCDOT spacing requirements.

Therefore, the extent of the roadway network analyzed consisted of the five project driveway intersections as well as the signalized intersection of Davison Road \& US 17/Savannah Highway.

According to the current development plan, based on the turn lane criteria in SCDOT's Roadway Design Manual, exclusive westbound/northbound left-turn lanes along County Line Road/Davison Road are recommended at Project Driveways \#1, \#2, \#3, and \#4 prior to full buildout of the development. However, as the development is built out and/or the development plan changes, a detailed, phased traffic study may be performed in the future to determine the precise timing and threshold of development triggering the need for turn lanes.

The results of the intersection analysis indicate that the study intersections (including the intersection of US 17/Savannah Highway \& Davison Road) currently operate and are expected to continue to operate at an acceptable LOS with full build out of the proposed Davison Investors development, with only one exception at one of the project driveways:

The intersection of Davison Road \& Ten Shillings Way/Project Driveway \#1 is anticipated to experience undesirable delay in the PM peak hour of the 2025 Build Conditions. However, this projected delay is likely due to the conservative nature of the HCM 2010 unsignalized methodology and is not an uncommon condition for two-way stop control during the peak hours of the day. Therefore, no improvements to mitigate this delay are recommended.

# DAVISON INVESTORS TRAFFIC IMPACT ANALYSIS APPENDICES 

## Appendix A TRIP GENERATION WORKSHEETS

## TRIP GENERATION ESTIMATES

Davison Investors Development
Weekday Daily


Weekday AM Peak Hour

| TRIP GENERATION CHARACTERISTICS |  |  |  | DIRECT. DISTRIB. |  | GROSS TRIPS |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | Ed. | LUC | Scale | Unit | Equation/Rate | In | Out | In | Out |
| Single-Family Detached <br> Housing | 10 th | 210 | 390 | DU | $\mathrm{T}=0.71(\mathrm{X})+4.80$ | $25 \%$ | $75 \%$ | 71 | 211 |
| Multifamily Housing <br> (Low-Rise) | 10 | 220 | 110 | DU | $\operatorname{Ln}(T)=0.95 \operatorname{Ln}(X)-0.51$ | $23 \%$ | $77 \%$ | 12 | 40 |

Weekday PM Peak Hour

| TRIP GENERATION CHARACTERISTICS |  |  |  |  |  |  |  |  | DIRECT. DISTRIB. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Land Use | Ed. | LUC | Scale | Unit | Equation/Rate | In | Out | In | Out |
| Gingle-Family Detached <br> Housing | 10 th | 210 | 390 | DU | $\operatorname{Ln}(T)=0.96 \operatorname{Ln}(X)+0.20$ | $63 \%$ | $37 \%$ | 236 | 139 |
| Multifamily Housing <br> (Low-Rise) | 10 | 220 | 110 | DU | $\operatorname{Ln}(T)=0.89 \operatorname{Ln}(X)-0.02$ | $63 \%$ | $37 \%$ | 40 | 24 |
|  |  | 64 |  |  |  |  |  |  |  |

## Appendix B TRAFFIC VOLUME DATA

(303) 216-2439
www.alltrafficdata.net


## Peak Hour - Pedestrians/Bicycles in Crosswalk



Note: Total study counts contained in parentheses.

## Traffic Counts

| Interval | BULOW LANDING RD Eastbound |  |  |  | BULOW LANDING RD <br> Westbound |  |  |  | DAVISON RD Northbound |  |  |  | DAVISON RD Southbound |  |  |  | Total | Rolling Hour | Pedestrain Crossings |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | U-Turn | Left | Thru | Right | U-Turn | Left | Thru |  | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right |  |  | West | East | South | North |
| 7:00 AM | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 1 | 0 | 0 | 16 | 1 | 0 | 0 | 54 | 0 | 76 | 366 | 0 | 0 | 0 | 0 |
| 7:15 AM | 0 | 0 | 0 | 0 | 0 | 9 | 0 | 0 | 0 | 0 | 20 | 3 | 0 | 1 | 63 | 0 | 96 | 366 | 0 | 0 | 0 | 0 |
| 7:30 AM | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 1 | 0 | 0 | 15 | 2 | 0 | 1 | 75 | 0 | 102 | 363 | 0 | 0 | 0 | 0 |
| 7:45 AM | 0 | 0 | 0 | 0 | 0 | 10 | 0 | 2 | 0 | 0 | 22 | 5 | 0 | 1 | 52 | 0 | 92 | 345 | 0 | 0 | 0 | 0 |
| 8:00 AM | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 2 | 0 | 0 | 15 | 4 | 0 | 3 | 47 | 0 | 76 | 323 | 0 | 0 | 0 | 0 |
| 8:15 AM | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 26 | 8 | 0 | 1 | 53 | 0 | 93 |  | 0 | 0 | 0 | 0 |
| 8:30 AM | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 24 | 2 | 0 | 0 | 55 | 0 | 84 |  | 0 | 0 | 0 | 0 |
| 8:45 AM | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 1 | 0 | 0 | 23 | 2 | 0 | 1 | 40 | 0 | 70 |  | 0 | 0 | 0 | 0 |

## Peak Rolling Hour Flow Rates

| Vehicle Type | Eastbound |  |  |  | Westbound |  |  |  | Northbound |  |  |  | Southbound |  |  |  | Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right |  |
| Articulated Trucks | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 5 | 0 | 9 |
| Lights | 0 | 0 | 0 | 0 | 0 | 31 | 0 | 4 | 0 | 0 | 48 | 11 | 0 | 2 | 210 | 0 | 306 |
| Mediums | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 21 | 0 | 0 | 1 | 29 | 0 | 51 |
| Total | 0 | 0 | 0 | 0 | 0 | 31 | 0 | 4 | 0 | 0 | 73 | 11 | 0 | 3 | 244 | 0 | 366 |

(303) 216-2439
www.alltrafficdata.net

Location: 2 DAVISON RD \& SAVANNAH HWY AM
Date and Start Time: Monday, August 26, 2019
Peak Hour: 07:00 AM - 08:00 AM
Peak 15-Minutes: 07:00 AM - 07:15 AM


## Peak Hour - Pedestrians/Bicycles in Crosswalk



Note: Total study counts contained in parentheses.
Traffic Counts

| Interval | SAVANNAH HWY <br> Eastbound |  |  |  | SAVANNAH HWY <br> Westbound |  |  |  | DAVISON RD <br> Northbound |  |  |  | DAVISON RD Southbound |  |  |  | Total | Rolling Hour | Pedestrain Crossings |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | U-Turn | Left | Thru | Right | U-Turn | Left | Thru |  | U-Turn | Left | Thru |  | U-Turn | Left | Thru | Right |  |  | West | East | South | North |
| 7:00 AM | 0 | 7 | 401 | 0 | 0 | 0 | 202 | 14 | 0 | 0 | 0 | 0 | 0 | 70 | 0 | 8 | 702 | 2,629 | 0 | 0 | 0 | 0 |
| 7:15 AM | 0 | 8 | 326 | 0 | 0 | 0 | 219 | 16 | 0 | 0 | 0 | 0 | 0 | 61 | 0 | 5 | 635 | 2,505 | 0 | 0 | 0 | 0 |
| 7:30 AM | 0 | 3 | 298 | 0 | 0 | 0 | 180 | 22 | 0 | 0 | 0 | 0 | 0 | 89 | 0 | 5 | 597 | 2,456 | 0 | 0 | 0 | 0 |
| 7:45 AM | 0 | 9 | 335 | 0 | 0 | 0 | 233 | 21 | 0 | 0 | 0 | 0 | 0 | 87 | 0 | 10 | 695 | 2,476 | 0 | 0 | 0 | 0 |
| 8:00 AM | 0 | 0 | 296 | 0 | 0 | 0 | 203 | 19 | 0 | 0 | 0 | 0 | 0 | 55 | 0 | 5 | 578 | 2,351 | 0 | 0 | 0 | 0 |
| 8:15 AM | 0 | 5 | 346 | 0 | 0 | 0 | 159 | 25 | 0 | 0 | 0 | 1 | 0 | 42 | 0 | 8 | 586 |  | 0 | 0 | 0 | 0 |
| 8:30 AM | 0 | 3 | 288 | 0 | 1 | 0 | 238 | 34 | 0 | 0 | 0 | 0 | 0 | 45 | 0 | 8 | 617 |  | 0 | 0 | 0 | 0 |
| 8:45 AM | 0 | 11 | 272 | 0 | 0 | 0 | 208 | 21 | 0 | 0 | 0 | 0 | 0 | 51 | 0 | 7 | 570 |  | 0 | 0 | 0 | 0 |

## Peak Rolling Hour Flow Rates

|  | Eastbound |  |  |  | Westbound |  |  |  | Northbound |  |  |  | Southbound |  |  |  | Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Vehicle Type | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right |  |
| Articulated Trucks | 0 | 1 | 41 | 0 | 0 | 0 | 42 | 5 | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 0 | 95 |
| Lights | 0 | 26 | 1,289 | 0 | 0 | 0 | 746 | 49 | 0 | 0 | 0 | 0 | 0 | 273 | 0 | 27 | 2,410 |
| Mediums | 0 | 0 | 30 | 0 | 0 | 0 | 46 | 19 | 0 | 0 | 0 | 0 | 0 | 28 | 0 | 1 | 124 |
| Total | 0 | 27 | 1,360 | 0 | 0 | 0 | 834 | 73 | 0 | 0 | 0 | 0 | 0 | 307 | 0 | 28 | 2,629 |

(303) 216-2439
www.alltrafficdata.net

Location: 1 DAVISON RD \& BULOW LANDING RD PM
Date and Start Time: Monday, August 26, 2019
Peak Hour: 05:00 PM - 06:00 PM
Peak 15-Minutes: 05:30 PM - 05:45 PM

## Peak Hour - All Vehicles



## Peak Hour - Pedestrians/Bicycles in Crosswalk



Note: Total study counts contained in parentheses.
Traffic Counts

| Interval | BULOW LANDING RD Eastbound |  |  |  | BULOW LANDING RD Westbound |  |  |  | DAVISON RD <br> Northbound |  |  |  |  | DAVISON RD Southbound |  |  |  | Total | Rolling Hour | Pedestrain Crossings |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | U-Turn | Left | Thru | Right | U-Turn | Left | Thru |  |  | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right |  |  | West | East | South | North |
| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 |  | 0 | 0 | 41 | 7 | 0 | 0 | 11 | 0 | 64 | 301 | 0 | 0 | 0 | 0 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 1 |  | 0 | 0 | 52 | 9 | 0 | 0 | 16 | 0 | 81 | 311 | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 |  | 0 | 0 | 37 | 8 | 0 | 2 | 20 | 0 | 71 | 313 | 0 | 0 | 0 | 0 |
| 4:45 PM | 0 | 0 | 0 | 0 | 1 | 5 | 0 | 0 |  | 0 | 0 | 53 | 8 | 0 | 0 | 18 | 0 | 85 | 337 | 0 | 0 | 0 | 0 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 |  | 0 | 0 | 47 | 4 | 0 | 0 | 19 | 0 | 74 | 338 | 0 | 0 | 0 | 0 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 0 |  | 0 | 0 | 48 | 7 | 0 | 0 | 22 | 0 | 83 |  | 0 | 0 | 0 | 0 |
| 5:30 PM | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 1 |  | 0 | 0 | 52 | 16 | 0 | 1 | 20 | 0 | 95 |  | 0 | 0 | 0 | 0 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 1 | 1 | 0 | 0 | 58 | 8 | 0 | 2 | 14 | 0 | 86 |  | 0 | 0 | 0 | 0 |

## Peak Rolling Hour Flow Rates

| Vehicle Type | Eastbound |  |  |  | Westbound |  |  |  | Northbound |  |  |  | Southbound |  |  |  | Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right |  |
| Articulated Trucks | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 4 |
| Lights | 0 | 0 | 0 | 0 | 0 | 16 | 0 | 4 | 0 | 0 | 195 | 35 | 0 | 3 | 74 | 0 | 327 |
| Mediums | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 1 | 0 | 7 |
| Total | 0 | 0 | 0 | 0 | 0 | 16 | 0 | 4 | 0 | 0 | 205 | 35 | 0 | 3 | 75 | 0 | 338 |

## All Traffic Data services $\operatorname{Inc} 10101$

(303) 216-2439
www.alltrafficdata.net

Location: 2 DAVISON RD \& SAVANNAH HWY PM
Date and Start Time: Monday, August 26, 2019
Peak Hour: 04:15 PM - 05:15 PM
Peak 15-Minutes: 05:00 PM - 05:15 PM


## Peak Hour - Pedestrians/Bicycles in Crosswalk



Note: Total study counts contained in parentheses.
Traffic Counts

| Interval | SAVANNAH HWY <br> Eastbound |  |  |  | SAVANNAH HWY <br> Westbound |  |  |  | DAVISON RD <br> Northbound |  |  |  | DAVISON RD <br> Southbound |  |  |  | Total | Rolling Hour | Pedestrain Crossings |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | U-Turn | Left | Thru | Right | U-Turn | eft | Thru |  | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right |  |  | West | East | South | North |
| 4:00 PM | 0 | 6 | 254 | 0 | 0 | 0 | 330 | 49 | 0 | 0 | 0 | 0 | 0 | 14 | 0 | 4 | 657 | 2,807 | 0 | 0 | 0 | 0 |
| 4:15 PM | 0 | 10 | 244 | 0 | 0 | 0 | 377 | 66 | 0 | 0 | 0 | 0 | 0 | 17 | 0 | 5 | 719 | 2,901 | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | 4 | 247 | 0 | 0 | 0 | 363 | 49 | 0 | 0 | 0 | 0 | 0 | 27 | 0 | 9 | 699 | 2,891 | 0 | 0 | 0 | 0 |
| 4:45 PM | 0 | 11 | 239 | 0 | 0 | 0 | 409 | 49 | 0 | 0 | 0 | 0 | 0 | 21 | 0 | 3 | 732 | 2,861 | 0 | 0 | 0 | 0 |
| 5:00 PM | 0 | 8 | 247 | 0 | 0 | 0 | 420 | 54 | 0 | 0 | 0 | 0 | 0 | 20 | 0 | 2 | 751 | 2,746 | 0 | 0 | 0 | 0 |
| 5:15 PM | 0 | 9 | 209 | 0 | 0 | 0 | 389 | 67 | 0 | 0 | 0 | 0 | 0 | 25 | 0 | 10 | 709 |  | 0 | 0 | 0 | 0 |
| 5:30 PM | 0 | 4 | 235 | 0 | 0 | 0 | 340 | 59 | 0 | 0 | 0 | 0 | 0 | 25 | 0 | 6 | 669 |  | 0 | 0 | 0 | 0 |
| 5:45 PM | 0 | 4 | 165 | 2 | 0 | 0 | 366 | 57 | 0 | 0 | 0 | 0 | 0 | 18 | 0 | 5 | 617 |  | 0 | 0 | 0 | 0 |

## Peak Rolling Hour Flow Rates

| Vehicle Type | Eastbound |  |  |  | Westbound |  |  |  | Northbound |  |  |  | Southbound |  |  |  | Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right | U-Turn | Left | Thru | Right |  |
| Articulated Trucks | 0 | 2 | 19 | 0 | 0 | 0 | 35 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 56 |
| Lights | 0 | 31 | 932 | 0 | 0 | 0 | 1,497 | 213 | 0 | 0 | 0 | 0 | 0 | 80 | 0 | 18 | 2,771 |
| Mediums | 0 | 0 | 26 | 0 | 0 | 0 | 37 | 5 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 1 | 74 |
| Total | 0 | 33 | 977 | 0 | 0 | 0 | 1,569 | 218 | 0 | 0 | 0 | 0 | 0 | 85 | 0 | 19 | 2,901 |

## Appendix C TRAFFIC VOLUME DEVELOPMENT WORKSHEETS

1 - US 17/Savannah Highway \& Davison Road


| 2 - Davison Road \& Ten Shillings Way |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | TOTAL PROJECT TRAFFIC |  |  |  |  |  |  |  |  |
| Traffic Control: TWSC <br> Date Counted: 8/26/2019 |  |  |  | AM | $\begin{aligned} & \text { IN } \\ & 83 \end{aligned}$ | OUT |  | $\begin{gathered} \text { IN } \\ 276 \end{gathered}$ | $\begin{aligned} & \text { OUT } \\ & 163 \end{aligned}$ |  |  |  |
| AM PEAK HOUR 7:00 AM - 8:00 AM | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| 2020 Existing Traffic Volumes | 0 | 0 | 0 | 35 | 0 | 6 | 0 | 85 | 12 | 2 | 281 | 0 |
| Years to Buildout | 5 | 5 | 5 | 5 |  | 5 | 5 | 5 | 5 | 5 | 5 | 5 |
| Yearly Growth Rate | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Background Traffic Vested Traffic | 0 | 0 | 0 | 4 | 0 | 1 | 0 | $\begin{gathered} 9 \\ 68 \end{gathered}$ | 1 | 0 | $\begin{gathered} 28 \\ 206 \end{gathered}$ | 0 |
| 2025 No Build Traffic Volumes | 0 | 0 | 0 | 39 | 0 | 7 | 0 | 162 | 13 | 2 | 515 | 0 |
| Inbound Project Traffic \% Outbound Project Traffic \% | 2\% |  | 10\% |  |  |  | 10\% | 75\% |  |  | 75\% | 2\% |
| 2025 Project Traffic 2025 Pass-By Traffic | 5 | 0 | 25 | 0 | 0 | 0 | 8 | 62 | 0 | 0 | 188 | 2 |
| 2025 Build Traffic Volumes | 5 | 0 | 25 | 39 | 0 | 7 | 8 | 224 | 13 | 2 | 703 | 2 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| PM PEAK HOUR <br> 5:00 PM - 6:00 PM | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| 2020 Existing Traffic Volumes | 0 | 0 | 0 | 23 | 0 | 4 | 0 | 245 | 38 | 7 | 93 | 0 |
| Years to Buildout | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 |
| Yearly Growth Rate | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Background Traffic | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 25 | 4 | 1 | 9 | 0 |
| Vested Traffic |  |  |  |  |  |  |  | 231 |  |  | 136 |  |
| 2025 No Build Traffic Volumes | 0 | 0 | 0 | 25 | 0 | 4 | 0 | 501 | 42 | 8 | 238 | 0 |
| Inbound Project Traffic \% |  |  |  |  |  |  | 10\% | 75\% |  |  |  | 2\% |
| Outbound Project Traffic \% | 2\% |  | 10\% |  |  |  |  |  |  |  | 75\% |  |
| 2025 Project Traffic 2025 Pass-By Traffic | 3 | 0 | 16 | 0 | 0 | 0 | 28 | 207 | 0 | 0 | 122 | 6 |
| 2025 Build Traffic Volumes | 3 | 0 | 16 | 25 | 0 | 4 | 28 | 708 | 42 | 8 | 360 | 6 |


| 3 - Davison Road \& DW\#2 |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Traffic Control: TWSC Date Counted: 8/26/2019 |  |  |  | TOTAL PROJECT TRAFFIC |  |  |  |  |  |  |  |  |
|  |  |  |  | AM |  | $\begin{aligned} & \text { OUT } \\ & 251 \end{aligned}$ | PM | $\begin{gathered} \text { IN } \\ 276 \end{gathered}$ | $\begin{gathered} \text { OUT } \\ 163 \end{gathered}$ |  |  |  |
| AM PEAK HOUR 7:00 AM - 8:00 AM | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| 2020 Existing Traffic Volumes | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 85 | 0 | 0 | 281 | 0 |
| Years to Buildout | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 |
| Yearly Growth Rate | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Background Traffic | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 | 0 | 0 | 28 | 0 |
| Vested Traffic |  |  |  |  |  |  |  | 68 |  |  | 206 |  |
| 2025 No Build Traffic Volumes | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 162 | 0 | 0 | 515 | 0 |
| Inbound Project Traffic \% Outbound Project Traffic \% | 2\% |  | 10\% |  |  |  | 10\% | $\begin{gathered} \hline 65 \% \\ 2 \% \end{gathered}$ |  |  | $\begin{gathered} \hline 2 \% \\ 65 \% \end{gathered}$ | 2\% |
| 2025 Project Traffic 2025 Pass-By Traffic | 5 | 0 | 25 | 0 | 0 | 0 | 8 | 59 | 0 | 0 | 165 | 2 |
| 2025 Build Traffic Volumes | 5 | 0 | 25 | 0 | 0 | 0 | 8 | 221 | 0 | 0 | 680 | 2 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| PM PEAK HOUR <br> 5:00 PM - 6:00 PM | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| 2020 Existing Traffic Volumes | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 245 | 0 | 0 | 93 | 0 |
| Years to Buildout | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 |
| Yearly Growth Rate | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Background Traffic | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 25 | 0 | 0 | 9 | 0 |
| Vested Traffic |  |  |  |  |  |  |  | 231 |  |  | 136 |  |
| 2025 No Build Traffic Volumes | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 501 | 0 | 0 | 238 | 0 |
| Inbound Project Traffic \% |  |  |  |  |  |  | 10\% | 65\% |  |  | 2\% | 2\% |
| Outbound Project Traffic \% | 2\% |  | 10\% |  |  |  |  | 2\% |  |  | 65\% |  |
| 2025 Project Traffic 2025 Pass-By Traffic | 3 | 0 | 16 | 0 | 0 | 0 | 28 | 182 | 0 | 0 | 112 | 6 |
| 2025 Build Traffic Volumes | 3 | 0 | 16 | 0 | 0 | 0 | 28 | 683 | 0 | 0 | 350 | 6 |


| 4 - Bulow Landing Road \& County Line Road |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | TOTAL PROJECT TRAFFIC |  |  |  |  |  | SBL | SBT | SBR |
|  |  |  |  |  | IN | OUT |  | $\begin{gathered} 1 \mathrm{~N} \\ 276 \end{gathered}$ | $\begin{aligned} & \text { OUT } \\ & 163 \end{aligned}$ |  |  |  |
| Date Counted: 8/26/2019 |  |  |  |  | 83 | 251 | PM |  |  |  |  |  |
| AM PEAK HOUR 7:00 AM - 8:00 AM | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR |  |  |  |
| 2020 Existing Traffic Volumes | 0 | 0 | 0 | 32 | 0 | 4 | 0 | 74 | 11 | 3 | 249 | 0 |
| Years to Buildout | 5 | 5 | 5 | 5 | 5 | 5 | 5 |  | 5 | 5 | 5 | 5 |
| Yearly Growth Rate | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Background Traffic | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 7 | 1 | 0 | 25 | 0 |
| Vested Traffic |  |  |  |  |  |  |  | 68 |  |  | 206 |  |
| 2025 No Build Traffic Volumes | 0 | 0 | 0 | 35 | 0 | 4 | 0 | 149 | 12 | 3 | 480 | 0 |
| Inbound Project Traffic \% Outbound Project Traffic \% | 5\% |  | 45\% |  |  |  | 45\% | $\begin{gathered} \hline 20 \% \\ 4 \% \end{gathered}$ |  |  | $4 \%$ $20 \%$ | 5\% |
|  | 12 | 0 | 113 | 0 | 0 | 0 | 37 | 27 | 0 | 0 |  | 4 |
| 2025 Pass-By Traffic |  |  |  |  |  |  |  |  |  |  | 5 | 4 |
| 2025 Build Traffic Volumes | 12 | 0 | 113 | 35 | 0 | 4 | 37 | 176 | 12 | 3 | 534 | 4 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| PM PEAK HOUR 5:00 PM - 6:00 PM | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| 2020 Existing Traffic Volumes | 0 | 0 | 0 | 16 | 0 | 4 | 0 | 209 | 36 | 3 | 77 | 0 |
| Years to Buildout | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 |
| Yearly Growth Rate | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Background Traffic | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 21 | 4 | 0 | 8 | 0 |
| Vested Traffic |  |  |  |  |  |  |  | 231 |  |  | 136 |  |
| 2025 No Build Traffic Volumes | 0 | 0 | 0 | 18 | 0 | 4 | 0 | 461 | 40 | 3 | 221 | 0 |
| Inbound Project Traffic \% |  |  |  |  |  |  | 45\% | 20\% |  |  | 4\% | 5\% |
| Outbound Project Traffic \% | 5\% |  | 45\% |  |  |  |  | 4\% |  |  | 20\% |  |
| 2025 Project Traffic 2025 Pass-By Traffic | 8 | 0 | 74 | 0 | 0 | 0 | 123 | 62 | 0 | 0 | 44 | 14 |
| 2025 Build Traffic Volumes | 8 | 0 | 74 | 18 | 0 | 4 | 123 | 523 | 40 | 3 | 265 | 14 |


| 5 - County Line Road \& DW\#4 |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Traffic Control: TWSC |  |  |  | TOTAL PROJECT TRAFFIC |  |  |  |  |  |  |  |  |
|  |  |  |  | AM |  | OUT |  | $\begin{gathered} \text { IN } \\ 276 \end{gathered}$ | $\begin{aligned} & \text { OUT } \\ & 163 \end{aligned}$ |  |  |  |
| AM PEAK HOUR 7:00 AM - 8:00 AM | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| 2020 Existing Traffic Volumes | 5 | 252 | 0 | 0 | 78 | 5 | 0 | 0 | 0 | 5 | 0 | 5 |
| Years to Buildout | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 |
| Yearly Growth Rate | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Background Traffic | 1 | 25 | 0 | 0 | 8 | 1 | 0 | 0 | 0 | 1 | 0 | 1 |
| Vested Traffic |  | 148 |  |  | 59 |  |  |  |  |  |  |  |
| 2025 No Build Traffic Volumes | 6 | 425 | 0 | 0 | 145 | 6 | 0 | 0 | 0 | 6 | 0 | 6 |
| Inbound Project Traffic \% |  | 9\% | 3\% | 15\% | 5\% |  |  |  |  |  |  |  |
| Outbound Project Traffic \% |  | 5\% |  |  | 9\% |  | 3\% |  | 15\% |  |  |  |
| 2025 Project Traffic 2025 Pass-By Traffic | 0 | 20 | 3 | 12 | 27 | 0 | 7 | 0 | 38 | 0 | 0 | 0 |
| 2025 Build Traffic Volumes | 6 | 445 | 3 | 12 | 172 | 6 | 7 | 0 | 38 | 6 | 0 | 6 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| PM PEAK HOUR <br> 5:00 PM - 6:00 PM | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| 2020 Existing Traffic Volumes | 5 | 80 | 0 | 0 | 213 | 5 | 0 | 0 | 0 | 5 | 0 | 5 |
| Years to Buildout | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 |
| Yearly Growth Rate | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Background Traffic | 1 | 8 | 0 | 0 | 21 | 1 | 0 | 0 | 0 | 1 | 0 | 1 |
| Vested Traffic |  | 107 |  |  | 169 |  |  |  |  |  |  |  |
| 2025 No Build Traffic Volumes | 6 | 195 | 0 | 0 | 403 | 6 | 0 | 0 | 0 | 6 | 0 | 6 |
| Inbound Project Traffic \% |  | 9\% | 3\% | 15\% | 5\% |  |  |  |  |  |  |  |
| Outbound Project Traffic \% |  | 5\% |  |  | 9\% |  | 3\% |  | 15\% |  |  |  |
| 2025 Project Traffic 2025 Pass-By Traffic | 0 | 33 | 8 | 41 | 29 | 0 | 5 | 0 | 25 | 0 | 0 | 0 |
| 2025 Build Traffic Volumes | 6 | 228 | 8 | 41 | 432 | 6 | 5 | 0 | 25 | 6 | 0 | 6 |


| 6 - County Line Road \& DW\#5 |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TOTAL PROJECT TRAFFIC |  |  |  |  |  |  |  |  |  |  |  |  |
| Traffic Control: TWSC <br> Date Counted: 8/26/2019 |  |  |  | AM | $\begin{aligned} & \text { IN } \\ & 83 \end{aligned}$ | OUT | PM | $\operatorname{IN}$ | OUT |  |  |  |
| AM PEAK HOUR <br> 7:00 AM - 8:00 AM | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| 2020 Existing Traffic Volumes | 0 | 252 | 0 | 0 | 78 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Years to Buildout | 5 |  | 5 | 5 | 5 | 5 |  | 5 | 5 | 5 | 5 | 5 |
| Yearly Growth Rate | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Background Traffic | 0 | 25 | 0 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Vested Traffic |  | 31 |  |  | 39 |  |  |  |  |  |  |  |
| 2025 No Build Traffic Volumes | 0 | 308 | 0 | 0 | 125 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Inbound Project Traffic \% Outbound Project Traffic \% |  | 12\% | 3\% | 5\% | 12\% |  | 3\% |  | 5\% |  |  |  |
| 2025 Project Traffic 2025 Pass-By Traffic | 0 | 10 | 3 | 4 | 30 | 0 | 8 | 0 | 13 | 0 | 0 | 0 |
| 2025 Build Traffic Volumes | 0 | 318 | 3 | 4 | 155 | 0 | 8 | 0 | 13 | 0 | 0 | 0 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| PM PEAK HOUR <br> 5:00 PM - 6:00 PM | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| 2020 Existing Traffic Volumes | 0 | 80 | 0 | 0 | 213 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Years to Buildout | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 |
| Yearly Growth Rate | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Background Traffic | 0 | 8 | 0 | 0 | 21 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Vested Traffic |  | 50 |  |  | 45 |  |  |  |  |  |  |  |
| 2025 No Build Traffic Volumes | 0 | 138 | 0 | 0 | 279 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Inbound Project Traffic \% |  | 12\% | 3\% | 5\% |  |  |  |  |  |  |  |  |
| Outbound Project Traffic \% |  |  |  | 12\% |  |  | 3\% |  | 5\% |  |  |  |
| 2025 Project Traffic 2025 Pass-By Traffic | 0 | 33 | 8 | 14 | 20 | 0 | 5 | 0 | 8 | 0 | 0 | 0 |
| 2025 Build Traffic Volumes | 0 | 171 | 8 | 14 | 299 | 0 | 5 | 0 | 8 | 0 | 0 | 0 |

## Appendix D ANALYSIS WORKSHEETS: 2020 EXISTING CONDITIONS



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.2 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | Mr |  | $\uparrow$ |  |  | $\uparrow$ |
| Traffic Vol, veh/h | 35 | 6 | 85 | 12 | 2 | 281 |
| Future Vol, veh/h | 35 | 6 | 85 | 12 | 2 | 281 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 2 | 2 | 7 | 7 | 7 | 7 |
| Mvmt Flow | 39 | 7 | 94 | 13 | 2 | 312 |



| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 1.1 |  |  |  |  |  |
| Movement W | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | * |  | 4 | 「 |  | $\uparrow$ |
| Traffic Vol, veh/h | 32 | 4 | 74 | 11 | 3 | 249 |
| Future Vol, veh/h | 32 | 4 | 74 | 11 | 3 | 249 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control S | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | 150 | - | - |
| Veh in Median Storage, \# | \# 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 2 | 2 | 7 | 7 | 7 | 7 |
| Mvmt Flow | 36 | 4 | 82 | 12 | 3 | 277 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |


| Major/Minor | Major1 |  | Major2 |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 93 | 0 | - | 0 | 382 | 90 |
| Stage 1 | - | - | - |  | 90 | - |
| Stage 2 | - | - | - | - | 292 | - |
| Critical Hdwy | 4.17 | - | - | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | 2.263 | - | - |  | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | 1471 | - | - |  | 620 | 968 |
| Stage 1 | - | - | - |  | 934 | - |
| Stage 2 | - | - | - | - | 758 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1471 | - | - | - | 617 | 968 |
| Mov Cap-2 Maneuver | - | - | - | - | 617 | - |
| Stage 1 | - | - | - |  | 929 | - |
| Stage 2 | - | - | - | - | 758 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | SB |  |
| HCM Control Delay, s | 0.1 |  | 0 |  | 9.8 |  |
| HCM LOS |  |  |  |  | A |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | EBL | EBT | WBT | WBR SBLn1 |  |
| Capacity (veh/h) |  | 1471 | - | - | - | 754 |
| HCM Lane V/C Ratio |  | 0.004 | - | - | - | 0.015 |
| HCM Control Delay (s) |  | 7.5 | 0 | - | - | 9.8 |
| HCM Lane LOS |  | A | A | - | - | A |
| HCM 95th \%tile Q(veh) |  | 0 | - | - | - | 0 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.9 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | Mr |  | F |  |  | $\uparrow$ |
| Traffic Vol, veh/h | 23 | 4 | 245 | 38 | 7 | 93 |
| Future Vol, veh/h | 23 | 4 | 245 | 38 | 7 | 93 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 89 | 89 | 89 | 89 | 89 | 89 |
| Heavy Vehicles, \% | 2 | 2 | 7 | 7 | 7 | 7 |
| Mvmt Flow | 26 | 4 | 275 | 43 | 8 | 104 |


| Major/Minor M | Minor1 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 417 | 297 | 0 | 0 | 318 | 0 |
| Stage 1 | 297 | - | - | - | - | - |
| Stage 2 | 120 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | - | - | 4.17 | - |
| Critical Hdwy Stg 1 | 5.42 |  | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | - | - | 2.263 | - |
| Pot Cap-1 Maneuver | 592 | 742 | - | - | 1214 | - |
| Stage 1 | 754 | - | - | - | - | - |
| Stage 2 | 905 | - | - | - | - | - |
| Platoon blocked, \% |  |  | - | - |  | - |
| Mov Cap-1 Maneuver | 588 | 742 | - | - | 1214 | - |
| Mov Cap-2 Maneuver | 588 | - | - | - | - | - |
| Stage 1 | 754 | - | - | - | - | - |
| Stage 2 | 899 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | WB |  | NB |  | SB |  |
| HCM Control Delay, s | 11.2 |  | 0 |  | 0.6 |  |
| HCM LOS | B |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NB | NBRWBLn1 |  | SBL | SBT |
| Capacity (veh/h) |  | - | - | 607 | 1214 | - |
| HCM Lane V/C Ratio |  | - | - | 0.05 | 0.006 | - |
| HCM Control Delay (s) |  | - | - | 11.2 | 8 | 0 |
| HCM Lane LOS |  | - | - | B | A | A |
| HCM 95th \%tile Q(veh) |  | - | - | 0.2 | 0 | - |


| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 0.7 |  |  |  |  |  |
| Movement W | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | * |  | 4 | 「 |  | $\uparrow$ |
| Traffic Vol, veh/h | 16 | 4 | 209 | 36 | 3 | 77 |
| Future Vol, veh/h | 16 | 4 | 209 | 36 | 3 | 77 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control S | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | 150 | - | - |
| Veh in Median Storage, \# | \# 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 89 | 89 | 89 | 89 | 89 | 89 |
| Heavy Vehicles, \% | 2 | 2 | 7 | 7 | 7 | 7 |
| Mvmt Flow | 18 | 4 | 235 | 40 | 3 | 87 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |


| Major/Minor | Major1 |  | Major2 |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 245 | 0 | - | 0 | 344 | 242 |
| Stage 1 | - | - | - | - | 242 | - |
| Stage 2 | - | - | - | - | 102 | - |
| Critical Hdwy | 4.17 | - | - | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | 2.263 | - | - | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | 1292 | - | - | - | 652 | 797 |
| Stage 1 | - | - | - | - | 798 | - |
| Stage 2 | - | - | - | - | 922 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1292 | - | - | - | 649 | 797 |
| Mov Cap-2 Maneuver | - | - | - | - | 649 | - |
| Stage 1 | - | - | - | - | 794 | - |
| Stage 2 | - | - | - | - | 922 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | SB |  |
| HCM Control Delay, s | 0.5 |  | 0 |  | 10.1 |  |
| HCM LOS |  |  |  |  | B |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | EBL | EBT | WBT | WBR SBLn1 |  |
| Capacity (veh/h) |  | 1292 | - | - | - | 715 |
| HCM Lane V/C Ratio |  | 0.004 | - | - | - | 0.016 |
| HCM Control Delay (s) |  | 7.8 | 0 | - | - | 10.1 |
| HCM Lane LOS |  | A | A | - | - | B |
| HCM 95th \%tile Q(veh |  | 0 | - | - | - | 0 |

## Appendix E ANALYSIS WORKSHEETS: 2025 NO BUILD CONDITIONS



| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 0.9 |  |  |  |  |  |
| Movement V | WBL | WBR | NBT | NBR | SBL |  |
| Lane Configurations | *F |  | $\hat{\beta}$ |  |  | $\uparrow$ |
| Traffic Vol, veh/h | 39 | 7 | 162 | 13 | 2 | 515 |
| Future Vol, veh/h | 39 | 7 | 162 | 13 | 2 | 515 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control Star | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | Stor | None | 仡 | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | \# 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 2 | 2 | 7 | 7 | 7 | 7 |
| Mvmt Flow | 43 | 8 | 180 | 14 | 2 | 572 |


| Major/Minor M | Minor1 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 763 | 187 | 0 | 0 | 194 | 0 |
| Stage 1 | 187 | - | - | - | - | - |
| Stage 2 | 576 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | - | - | 4.17 | - |
| Critical Hdwy Stg 1 | 5.42 |  | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | - | - | 2.263 | - |
| Pot Cap-1 Maneuver | 372 | 855 | - | - | 1350 | - |
| Stage 1 | 845 | - | - | - | - | - |
| Stage 2 | 562 | - | - | - | - | - |
| Platoon blocked, \% |  |  | - | - |  | - |
| Mov Cap-1 Maneuver | 371 | 855 | - | - | 1350 | - |
| Mov Cap-2 Maneuver | 371 | - | - | - | - | - |
| Stage 1 | 845 | - | - | - | - | - |
| Stage 2 | 561 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | WB |  | NB |  | SB |  |
| HCM Control Delay, s | 15.1 |  | 0 |  | 0 |  |
| HCM LOS | C |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBT | NBRWBLn1 |  | SBL | SBT |
| Capacity (veh/h) |  | - | - | 406 | 1350 | - |
| HCM Lane V/C Ratio |  | - | - | 0.126 | 0.002 | - |
| HCM Control Delay (s) |  | - | - | 15.1 | 7.7 | 0 |
| HCM Lane LOS |  | - | - | C | A | A |
| HCM 95th \%tile Q(veh) |  | - | - | 0.4 | 0 | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.8 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | Mr |  | 个 | $\mathbf{7}$ |  | $\neq$ |
| Traffic Vol, veh/h | 35 | 4 | 149 | 12 | 3 | 480 |
| Future Vol, veh/h | 35 | 4 | 149 | 12 | 3 | 480 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | 150 | - | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 2 | 2 | 7 | 7 | 7 | 7 |
| Mvmt Flow | 39 | 4 | 166 | 13 | 3 | 533 |



| Intersection |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 0.3 |  |  |  |  |  |  |
| Movement EBL EBT WBT WBR SBL SBR |  |  |  |  |  |  |  |
| Lane Configurations $\uparrow \uparrow \hat{\beta}$ |  |  |  |  |  |  |  |
| Traffic Vol, veh/h | 6 | 425 | 145 | 6 |  | 6 |  |
| Future Vol, veh/h | 6 | 425 | 145 | 6 | 6 | 6 |  |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Sign Control Free Free Free Free Stop Stop |  |  |  |  |  |  |  |
| RT Channelized - None - None - None |  |  |  |  |  |  |  |
|  | - | - | - | - | 0 | - |  |
| Veh in Median Storage, \# |  | 0 | 0 | - | 0 | - |  |
| Grade, \% |  | 0 | 0 | - | 0 | - |  |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 |  |
| Heavy Vehicles, \% | 2 | 2 | 7 | 7 | 7 | 7 |  |
| Mvmt Flow | 7 | 472 | 161 | 7 | 7 | 7 |  |


| Major/Minor $\quad$ N | Major1 |  | Major2 |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 168 | 0 | - | 0 | 651 | 165 |
| Stage 1 | - | - | - | - | 165 | - |
| Stage 2 | - | - | - | - | 486 | - |
| Critical Hdwy | 4.12 | - | - | - | 6.47 | 6.27 |
| Critical Hdwy Stg 1 | - | - | - |  | 5.47 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.47 | - |
| Follow-up Hdwy | 2.218 | - | - |  | 3.563 | 3.363 |
| Pot Cap-1 Maneuver | 1410 | - | - |  | 425 | 867 |
| Stage 1 | - | - | - |  | 852 | - |
| Stage 2 | - | - | - |  | 608 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1410 | - | - | - | 422 | 867 |
| Mov Cap-2 Maneuver | - | - | - |  | 422 | - |
| Stage 1 | - | - | - |  | 846 | - |
| Stage 2 | - | - | - |  | 608 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | SB |  |
| HCM Control Delay, s | 0.1 |  | 0 |  | 11.5 |  |
| HCM LOS |  |  |  |  | B |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | EBL | EBT | WBT | WBR SBLn1 |  |
| Capacity (veh/h) |  | 1410 | - |  | - | 568 |
| HCM Lane V/C Ratio |  | 0.005 | - | - | - | 0.023 |
| HCM Control Delay (s) |  | 7.6 | 0 | - | - | 11.5 |
| HCM Lane LOS |  | A | A | - | - | B |
| HCM 95th \%tile Q(veh) |  | 0 | - | - | - | 0.1 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.7 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | P |  | $\uparrow$ |  |  | $\uparrow$ |
| Traffic Vol, veh/h | 25 | 4 | 501 | 42 | 8 | 238 |
| Future Vol, veh/h | 25 | 4 | 501 | 42 | 8 | 238 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 2 | 2 | 7 | 7 | 7 | 7 |
| Mvmt Flow | 28 | 4 | 557 | 47 | 9 | 264 |


| Major/Minor | Minor1 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 863 | 581 | 0 | 0 | 604 | 0 |
| Stage 1 | 581 | - | - | - | - | - |
| Stage 2 | 282 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | - | - | 4.17 | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | - | - | 2.263 | - |
| Pot Cap-1 Maneuver | 325 | 514 | - | - | 950 | - |
| Stage 1 | 559 | - | - | - | - | - |
| Stage 2 | 766 | - | - | - | - | - |
| Platoon blocked, \% |  |  | - | - |  | - |
| Mov Cap-1 Maneuver | 321 | 514 | - | - | 950 | - |
| Mov Cap-2 Maneuver | 321 | - | - | - | - | - |
| Stage 1 | 559 | - | - | - | - | - |
| Stage 2 | 758 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | WB |  | NB |  | SB |  |
| HCM Control Delay, s | 16.7 |  | 0 |  | 0.3 |  |
| HCM LOS | C |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBT | NBRWBLn1 |  | SBL | SBT |
| Capacity (veh/h) |  | - | - | 339 | 950 | - |
| HCM Lane V/C Ratio |  | - | - | 0.095 | 0.009 | - |
| HCM Control Delay (s) |  | - | - | 16.7 | 8.8 | 0 |
| HCM Lane LOS |  | - | - | C | A | A |
| HCM 95th \%tile Q(veh) |  | - | - | 0.3 | 0 | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.5 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | Mr |  | 个 | $\mathbf{F}$ |  | $\neq 1$ |
| Traffic Vol, veh/h | 18 | 4 | 461 | 40 | 3 | 221 |
| Future Vol, veh/h | 18 | 4 | 461 | 40 | 3 | 221 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | 150 | - | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 2 | 2 | 7 | 7 | 7 | 7 |
| Mvmt Flow | 20 | 4 | 512 | 44 | 3 | 246 |


| Major/Minor | Minor1 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 764 | 512 | 0 | 0 | 556 | 0 |
| Stage 1 | 512 | - | - | - | - | - |
| Stage 2 | 252 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | - | - | 4.17 | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | - | - | 2.263 | - |
| Pot Cap-1 Maneuver | 372 | 562 | - | - | 990 | - |
| Stage 1 | 602 | - | - | - | - | - |
| Stage 2 | 790 | - | - | - | - | - |
| Platoon blocked, \% |  |  | - | - |  | - |
| Mov Cap-1 Maneuver | 371 | 562 | - | - | 990 | - |
| Mov Cap-2 Maneuver | 371 | - | - | - | - | - |
| Stage 1 | 602 | - | - | - | - | - |
| Stage 2 | 787 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | WB |  | NB |  | SB |  |
| HCM Control Delay, s | 14.7 |  | 0 |  | 0.1 |  |
| HCM LOS | B |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBT | NBRWBLn1 |  | SBL | SBT |
| Capacity (veh/h) |  | - | - | 395 | 990 | - |
| HCM Lane V/C Ratio |  | - | - | 0.062 | 0.003 | - |
| HCM Control Delay (s) |  | - | - | 14.7 | 8.6 | 0 |
| HCM Lane LOS |  | - | - | B | A | A |
| HCM 95th \%tile Q(veh) |  | - | - | 0.2 | 0 | - |


| Intersection |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 0.3 |  |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |  |
| Lane Configurations $\quad$ ¢ |  |  |  |  |  |  |  |
| Traffic Vol, veh/h | 6 | 195 | 403 | 6 |  | 6 |  |
| Future Vol, veh/h | 6 | 195 | 403 | 6 | 6 | 6 |  |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Sign Control Free Free Free Free Stop Stop |  |  |  |  |  |  |  |
| RT Channelized - None - None - None |  |  |  |  |  |  |  |
|  | - | - | - | - | 0 | - |  |
| Veh in Median Storage, \# |  | 0 | 0 | - | 0 | - |  |
| Grade, \% |  | 0 | 0 | - | 0 | - |  |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 |  |
| Heavy Vehicles, \% | 2 | 2 | 7 | 7 | 7 | 7 |  |
| Mvmt Flow | 7 | 217 | 448 | 7 | 7 | 7 |  |


| Major/Minor | Major1 | Major2 |  | Minor2 |  |  |
| :--- | ---: | :--- | ---: | :--- | ---: | ---: |
| Conflicting Flow All | 455 | 0 | - | 0 | 683 | 452 |
| $\quad$ Stage 1 | - | - | - | - | 452 | - |
| Stage 2 | - | - | - | - | 231 | - |
| Critical Hdwy | 4.12 | - | - | -6.47 | 6.27 |  |
| Critical Hdwy Stg 1 | - | - | - | - | 5.47 | - |
| Critical Hdwy Stg 2 | - | - | - | -5.47 | - |  |
| Follow-up Hdwy | 2.218 | - | - | -3.563 | 3.363 |  |
| Pot Cap-1 Maneuver | 1106 | - | - | - | 407 | 597 |
| $\quad$ Stage 1 | - | - | - | - | 631 | - |
| $\quad$ Stage 2 | - | - | - | - | 796 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1106 | - | - | - | 404 | 597 |
| Mov Cap-2 Maneuver | - | - | - | - | 404 | - |
| Stage 1 | - | - | - | - | 627 | - |
| Stage 2 | - | - | - | - | 796 | - |


| Approach | EB | WB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0.2 | 0 | 12.7 |
| HCM LOS |  |  | B |


| Minor Lane/Major Mvmt | EBL | EBT | WBT | WBR SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1106 | - | - | -482 |
| HCM Lane V/C Ratio | 0.006 | - | - | -0.028 |
| HCM Control Delay (s) | 8.3 | 0 | - | -12.7 |
| HCM Lane LOS | A | A | - | - |
| HCM 95th \%tile Q(veh) | 0 | - | - | - |

## Appendix F ANALYSIS WORKSHEETS: 2025 BUILD CONDITIONS





| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 3.8 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | \& |  |  | \& |  |  | $\uparrow$ | 「 |  | \& |  |
| Traffic Vol, veh/h | 12 | 0 | 113 | 35 | 0 | 4 | 37 | 176 | 12 | 3 | 534 | 4 |
| Future Vol, veh/h | 12 | 0 | 113 | 35 | 0 | 4 | 37 | 176 | 12 | 3 | 534 | 4 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control S | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | 150 | - | - | - |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 7 | 7 | 7 | 7 | 7 | 7 |
| Mvmt Flow | 13 | 0 | 126 | 39 | 0 | 4 | 41 | 196 | 13 | 3 | 593 | 4 |



5: Project Driveway \#4/Equestrian Center \& County Line Road



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.5 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | F |  |  | -1 | Mr |  |
| Traffic Vol, veh/h | 318 | 3 | 4 | 155 | 8 | 13 |
| Future Vol, veh/h | 318 | 3 | 4 | 155 | 8 | 13 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 7 | 7 | 7 | 7 | 2 | 2 |
| Mvmt Flow | 353 | 3 | 4 | 172 | 9 | 14 |


| Major/Minor M | Major1 |  | Major2 |  | Minor1 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 0 | 0 | 356 | 0 | 535 | 355 |
| Stage 1 | - | - | - | - | 355 | - |
| Stage 2 | - | - | - | - | 180 | - |
| Critical Hdwy | - | - | 4.17 | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | - | - | 2.263 | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | - | - | 1175 | - | 506 | 689 |
| Stage 1 | - | - | - | - | 710 | - |
| Stage 2 | - | - | - | - | 851 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 1175 | - | 504 | 689 |
| Mov Cap-2 Maneuver | - | - | - | - | 504 | - |
| Stage 1 | - | - | - | - | 710 | - |
| Stage 2 | - | - | - | - | 848 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | NB |  |
| HCM Control Delay, s | 0 |  | 0.2 |  | 11.2 |  |
| HCM LOS |  |  |  |  | B |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBLn1 | EBT | EBR | WBL WBT |  |
| Capacity (veh/h) |  | 604 | - | - | 1175 | - |
| HCM Lane V/C Ratio |  | 0.039 | - | - | 0.004 | - |
| HCM Control Delay (s) |  | 11.2 | - | - | 8.1 | 0 |
| HCM Lane LOS |  | B | - | - | A | A |
| HCM 95th \%tile Q(veh) |  | 0.1 | - | - | 0 | - |


|  | $\rangle$ |  | 4 | 4 | $\downarrow$ | $\checkmark$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBT | WBR | SBL | SBR |  |
| Lane Configurations | \％ | 个4 | 个个 | 「 | ${ }^{*}$ | 「 |  |
| Traffic Volume（vph） | 118 | 1097 | 1760 | 629 | 322 | 69 |  |
| Future Volume（vph） | 118 | 1097 | 1760 | 629 | 322 | 69 |  |
| Turn Type | Prot | NA | NA | Perm | Prot | Perm |  |
| Protected Phases | 1 | Free！ | 2 |  | $8!$ |  |  |
| Permitted Phases |  |  |  | 2 |  | 8 |  |
| Detector Phase | 1 |  | 2 | 2 | 8 | 8 |  |
| Switch Phase |  |  |  |  |  |  |  |
| Minimum Initial（s） | 6.0 |  | 20.0 | 20.0 | 8.0 | 8.0 |  |
| Minimum Split（s） | 12.0 |  | 27.0 | 27.0 | 14.5 | 14.5 |  |
| Total Split（s） | 15.0 |  | 73.0 | 73.0 | 32.0 | 32.0 |  |
| Total Split（\％） | 12．5\％ |  | 60．8\％ | 60．8\％ | 26．7\％ | 26．7\％ |  |
| Yellow Time（s） | 4.0 |  | 5.0 | 5.0 | 4.0 | 4.0 |  |
| All－Red Time（s） | 2.0 |  | 2.0 | 2.0 | 2.5 | 2.5 |  |
|  | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Lost Time Adjust（s） Total Lost Time（s） | 6.0 |  | 7.0 | 7.0 | 6.5 | 6.5 |  |
| Lead／Lag | Lead |  | Lag | Lag |  |  |  |
| Lead－Lag Optimize？ | Yes |  | Yes | Yes |  |  |  |
| Recall Mode | Min |  | Min | Min | Min | Min |  |
| Act Efftt Green（s） | 9.0 | 119.8 | 66.0 | 66.0 | 25.3 | 25.3 |  |
| Actuated g／C Ratio | 0.08 | 1.00 | 0.55 | 0.55 | 0.21 | 0.21 |  |
| v／c Ratio | 0.97 | 0.34 | 0.98 | 0.64 | 0.95 | 0.21 |  |
| Control Delay | 126.5 | 0.3 | 42.9 | 9.7 | 84.5 | 21.4 |  |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Total Delay | 126.5 | 0.3 | 42.9 | 9.7 | 84.5 | 21.4 |  |
| LOS | F | A | D | A | F | C |  |
| Approach Delay |  | 12.5 | 34.1 |  | 73.3 |  |  |
| Approach LOS |  | B | C |  | E |  |  |
| Intersection Summary |  |  |  |  |  |  |  |
| Cycle Length： 120 |  |  |  |  |  |  |  |
| Actuated Cycle Length： 119.8 |  |  |  |  |  |  |  |
| Natural Cycle： 110 |  |  |  |  |  |  |  |
| Control Type：Actuated－Uncoordinated |  |  |  |  |  |  |  |
| Maximum v／c Ratio： 0.98 |  |  |  |  |  |  |  |
| Intersection Signal D |  |  |  |  | ersectio | LOS：C |  |
| Intersection Capacity Utilization 89．3\％Analysis Period（min） 15 |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
| ！Phase conflict between lane groups． |  |  |  |  |  |  |  |
| Splits and Phases：1：US17／Savannah Hwy \＆Davison Road |  |  |  |  |  |  |  |
|  | Ø2 |  |  |  |  |  |  |
| 15 s  73 |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  | ${ }^{\circ}$ |
|  |  |  |  |  |  |  | 32 s |




| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 2.7 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | \& |  |  | \$ |  |  | $\uparrow$ | 「 |  | \& |  |
| Traffic Vol, veh/h | 8 | 0 | 74 | 18 | 0 | 4 | 123 | 523 | 40 | 3 | 265 | 14 |
| Future Vol, veh/h | 8 | 0 | 74 | 18 | 0 | 4 | 123 | 523 | 40 | 3 | 265 | 14 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | 150 | - | - | - |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 7 | 7 | 7 | 7 | 7 | 7 |
| Mvmt Flow | 9 | 0 | 82 | 20 | 0 | 4 | 137 | 581 | 44 | 3 | 294 | 16 |






| Major/Minor $\quad$ N | Major1 |  | Major2 |  | Minor1 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 0 | 0 | 199 | 0 | 559 | 195 |
| Stage 1 | - | - | - | - | 195 | - |
| Stage 2 | - | - | - | - | 364 | - |
| Critical Hdwy | - | - | 4.17 | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - |  | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | - |  | 2.263 |  | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | - | - | 1344 | - | 490 | 846 |
| Stage 1 | - | - | - |  | 838 | - |
| Stage 2 | - | - | - |  | 703 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 1344 | - | 483 | 846 |
| Mov Cap-2 Maneuver | - | - | - |  | 483 | - |
| Stage 1 | - | - | - |  | 838 | - |
| Stage 2 | - | - | - |  | 692 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | NB |  |
| HCM Control Delay, s | 0 |  | 0.3 |  | 10.6 |  |
| HCM LOS |  |  |  |  | B |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) |  | 656 | - | - | 1344 | - |
| HCM Lane V/C Ratio |  | 0.022 | - |  | 0.012 | - |
| HCM Control Delay (s) |  | 10.6 | - | - | 7.7 | 0 |
| HCM Lane LOS |  | B | - | - | A | A |
| HCM 95th \%tile Q(veh) |  | 0.1 | - | - | 0 | - |

## Appendix G ANALYSIS WORKSHEETS: 2025 BUILD CONDITIONS W/ RECOMMENDED IMPROVEMENTS



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 1.8 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |  |
| Lane Configurations |  | ¢ |  |  | $\dagger$ |  | \% | $\hat{6}$ |  | \% | $\uparrow$ |  |  |
| Traffic Vol, veh/h | 5 | 0 | 25 | 39 | 0 | 7 | 8 | 224 | 13 | 2 | 703 | 2 |  |
| Future Vol, veh/h | 5 | 0 | 25 | 39 | 0 | 7 | 8 | 224 | 13 | 2 | 703 | 2 |  |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |  |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |  |
| Storage Length | - | - | - | - | - | - | 200 | - | - | 200 | - | - |  |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |  |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 7 | 7 | 7 | 7 | 7 | 7 |  |
| Mvmt Flow | 6 | 0 | 28 | 43 | 0 | 8 | 9 | 249 | 14 | 2 | 781 | 2 |  |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |








| Major/Minor M | Major1 |  | Major2 |  | Minor1 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 0 | 0 | 356 | 0 | 535 | 355 |
| Stage 1 | - | - | - | - | 355 | - |
| Stage 2 | - | - | - | - | 180 | - |
| Critical Hdwy | - | - | 4.17 | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | - | - | 2.263 | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | - | - | 1175 | - | 506 | 689 |
| Stage 1 | - | - | - | - | 710 | - |
| Stage 2 | - | - | - | - | 851 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 1175 | - | 504 | 689 |
| Mov Cap-2 Maneuver | - | - | - | - | 504 | - |
| Stage 1 | - | - | - | - | 710 | - |
| Stage 2 | - | - | - | - | 848 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | NB |  |
| HCM Control Delay, s | 0 |  | 0.2 |  | 11.2 |  |
| HCM LOS |  |  |  |  | B |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBLn1 | EBT | EBR | WBL WBT |  |
| Capacity (veh/h) |  | 604 | - | - | 1175 | - |
| HCM Lane V/C Ratio |  | 0.039 | - | - | 0.004 | - |
| HCM Control Delay (s) |  | 11.2 | - | - | 8.1 | 0 |
| HCM Lane LOS |  | B | - | - | A | A |
| HCM 95th \%tile Q(veh) |  | 0.1 | - | - | 0 | - |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 1.4 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | * |  |  | \& |  | ${ }^{7}$ | $\uparrow$ |  | ${ }^{1 /}$ | $\uparrow$ |  |
| Traffic Vol, veh/h | 3 | 0 | 16 | 25 | 0 | 4 | 28 | 708 | 42 | 8 | 360 | 6 |
| Future Vol, veh/h | 3 | 0 | 16 | 25 | 0 | 4 | 28 | 708 | 42 | 8 | 360 | 6 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | 200 | - | - | 200 | - | - |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 7 | 7 | 7 | 7 | 7 | 7 |
| Mvmt Flow | 3 | 0 | 18 | 28 | 0 | 4 | 31 | 787 | 47 | 9 | 400 | 7 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.4 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | r |  | 1 | 4 | $\uparrow$ |  |
| Traffic Vol, veh/h | 3 | 16 | 28 | 683 | 350 | 6 |
| Future Vol, veh/h | 3 | 16 | 28 | 683 | 350 | 6 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | 200 | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 2 | 2 | 7 | 7 | 7 | 7 |
| Mvmt Flow | 3 | 18 | 31 | 759 | 389 | 7 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 2.7 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ¢ |  |  | $\dagger$ |  | ${ }^{7}$ | 4 | 「 | ${ }^{7}$ | $\hat{1}$ |  |
| Traffic Vol, veh/h | 8 | 0 | 74 | 18 | 0 | 4 | 123 | 523 | 40 | 3 | 265 | 14 |
| Future Vol, veh/h | 8 | 0 | 74 | 18 | 0 | 4 | 123 | 523 | 40 | 3 | 265 | 14 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control Stoper | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | 200 | - | 150 | 200 | - | - |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 7 | 7 | 7 | 7 | 7 | 7 |
| Mvmt Flow | 9 | 0 | 82 | 20 | 0 | 4 | 137 | 581 | 44 | 3 | 294 | 16 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 1.2 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | $\uparrow$ |  | ${ }^{*}$ | $\uparrow$ |  |  | \& |  |  | $\uparrow$ |  |
| Traffic Vol, veh/h | 6 | 228 | 8 | 41 | 432 | 6 | 5 | 0 | 25 | 6 | 0 | 6 |
| Future Vol, veh/h | 6 | 228 | 8 | 41 | 432 | 6 | 5 | 0 | 25 | 6 | 0 | 6 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control Froser | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | 200 | - | - | 200 | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 7 | 7 | 7 | 7 | 7 | 7 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 7 | 253 | 9 | 46 | 480 | 7 | 6 | 0 | 28 | 7 | 0 | 7 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.5 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\uparrow$ |  |  | $\uparrow$ | MF |  |
| Traffic Vol, veh/h | 171 | 8 | 14 | 299 | 5 | 8 |
| Future Vol, veh/h | 171 | 8 | 14 | 299 | 5 | 8 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 7 | 7 | 7 | 7 | 2 | 2 |
| Mvmt Flow | 190 | 9 | 16 | 332 | 6 | 9 |


| Major/Minor | Major1 |  | Major2 |  | Minor1 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 0 | 0 | 199 | 0 | 559 | 195 |
| Stage 1 | - | - | - | - | 195 | - |
| Stage 2 | - | - | - | - | 364 | - |
| Critical Hdwy | - | - | 4.17 | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | - | - | 2.263 | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | - | - | 1344 | - | 490 | 846 |
| Stage 1 | - | - | - | - | 838 | - |
| Stage 2 | - | - | - | - | 703 | - |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 1344 | - | 483 | 846 |
| Mov Cap-2 Maneuver | - | - | - | - | 483 | - |
| Stage 1 | - | - | - | - | 838 | - |
| Stage 2 | - | - | - | - | 692 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | NB |  |
| HCM Control Delay, s | 0 |  | 0.3 |  | 10.6 |  |
| HCM LOS |  |  |  |  | B |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBLn1 EBT EBR WBL WBT |  |  |  |  |
| Capacity (veh/h) |  | 656 | - | - | 1344 | - |
| HCM Lane V/C Ratio |  | 0.022 | - | - | 0.012 | - |
| HCM Control Delay (s) |  | 10.6 | - | - | 7.7 | 0 |
| HCM Lane LOS |  | B | - | - | A | A |
| HCM 95th \%tile Q(veh) |  | 0.1 | - | - | 0 | - |

## Appendix H TURN LANE ANALYSIS WORKSHEETS

INTERSECTION: County Line Road \& Project Driveway 1
MOVEMENT: Southbound Right-Turn Lane


Note: For highways with a design speed below 50 miles per hour with a DHV $<300$ and where right turns $>40$, an adjustment should be used. To read the vertical axis of the chart, subtract 20 from the actual number of right turns.

## Example

Design Speed $\quad=\quad 35$ miles per hour DHV $\quad=\quad 250$ vehicles per hour Right Turns $\quad=\quad 100$ vehicles per hour

Problem: Determine if a right-turn lane is necessary.
Solution: $\quad$ To read the vertical axis, use $100-20=80$ vehicles per hour. The figure indicates that a right-turn lane is not necessary, unless other factors (e.g., high crash rate) indicate a lane is needed.

GUIDELINES FOR RIGHT-TURN LANES AT UNSIGNALIZED INTERSECTIONS ON TWO-LANE HIGHWAYS

Figure 9.5-A

| 2025 Build <br> Conditions | Major Road Volume (Direction <br> of Right Turn Ingress) | Right Turn <br> Volume | Speed along <br> Right Turn <br> Ingress | Symbol |
| :---: | :---: | :---: | :---: | :---: |
| AM Peak Hour | 707 | 2 | 45 | 0 |
| PM Peak Hour | 374 | 6 | 45 | $\square$ |

INTERSECTION: County Line Road \& Project Driveway 1
MOVEMENT: Northbound Left-Turn Lane
9.5-8 INTERSECTIONS March 2017


## Instructions:

1. The family of curves represents the percent of left turns in the advancing volume ( $V_{A}$ ). The designer should locate the curve for the actual percentage of left turns. When this is not an even increment of 5, the designer should estimate where the curve lies.
2. Read $V_{A}$ and $V_{O}$ into the chart and locate the intersection of the two volumes.
3. Note the location of the point in \#2 relative to the line in \#1. If the point is to the right of the line, then a left-turn lane is warranted. If the point is to the left of the line, then a leftturn lane is not warranted based on traffic volumes.

VOLUME GUIDELINES FOR LEFT-TURN LANES AT UNSIGNALIZED INTERSECTIONS ON TWO-LANE HIGHWAYS ( 45 mph )

Figure 9.5-F

| 2025 Build <br> Conditions | $\mathbf{V}_{\mathrm{A}}$ | EBL | $\mathbf{V}_{\mathbf{O}}$ | $\mathbf{V}_{\mathrm{A}}$ LT \% | Symbol |
| :---: | :---: | :---: | :---: | :---: | :---: |
| AM Peak Hour | 245 | 8 | 707 | $3.3 \%$ | 0 |
| PM Peak Hour | 778 | 28 | 374 | $3.6 \%$ | $\square$ |

INTERSECTION: County Line Road \& Project Driveway 2
MOVEMENT: Southbound Right-Turn Lane


Note: For highways with a design speed below 50 miles per hour with a DHV <300 and where right turns $>40$, an adjustment should be used. To read the vertical axis of the chart, subtract 20 from the actual number of right turns.

## Example

Given:

| Design Speed | $=$ | 35 miles per hour |
| :--- | :--- | :--- |
| DHV | $=$ | 250 vehicles per hour |
| Right Turns | $=$ | 100 vehicles per hour |

Problem: Determine if a right-turn lane is necessary.
Solution: $\quad$ To read the vertical axis, use $100-20=80$ vehicles per hour. The figure indicates that a right-turn lane is not necessary, unless other factors (e.g., high crash rate) indicate a lane is needed.

GUIDELINES FOR RIGHT-TURN LANES AT UNSIGNALIZED INTERSECTIONS ON TWO-LANE HIGHWAYS

Figure 9.5-A

| 2025 Build <br> Conditions | Major Road Volume (Direction <br> of Right Turn Ingress) | Right Turn <br> Volume | Speed along <br> Right Turn <br> Ingress | Symbol |
| :---: | :---: | :---: | :---: | :---: |
| AM Peak Hour | 682 | 6 | 45 | 0 |
| PM Peak Hour | 356 | 2 | 45 | $\square$ |

INTERSECTION: County Line Road \& Project Driveway 2
MOVEMENT: Northbound Left-Turn Lane
9.5-8 INTERSECTIONS March 2017


## Instructions:

1. The family of curves represents the percent of left turns in the advancing volume ( $V_{A}$ ). The designer should locate the curve for the actual percentage of left turns. When this is not an even increment of 5, the designer should estimate where the curve lies.
2. Read $V_{A}$ and $V_{O}$ into the chart and locate the intersection of the two volumes.
3. Note the location of the point in \#2 relative to the line in \#1. If the point is to the right of the line, then a left-turn lane is warranted. If the point is to the left of the line, then a leftturn lane is not warranted based on traffic volumes.

VOLUME GUIDELINES FOR LEFT-TURN LANES AT UNSIGNALIZED INTERSECTIONS ON TWO-LANE HIGHWAYS (45 mph)

Figure 9.5-F

| 2025 Build <br> Conditions | $\mathbf{V A}_{\text {A }}$ | EBL | $\mathbf{V}_{\mathbf{O}}$ | $\mathbf{V}_{\text {A }}$ LT \% | Symbol |
| :---: | :---: | :---: | :---: | :---: | :---: |
| AM Peak Hour | 229 | 8 | 682 | $3.5 \%$ | 0 |
| PM Peak Hour | 711 | 28 | 356 | $3.9 \%$ | $\square$ |

INTERSECTION: County Line Road \& Project Driveway 3
MOVEMENT: Southbound Right-Turn Lane


Note: For highways with a design speed below 50 miles per hour with a DHV $<300$ and where right turns $>40$, an adjustment should be used. To read the vertical axis of the chart, subtract 20 from the actual number of right turns.

## Example

Design Speed $\quad=\quad 35$ miles per hour DHV $=\quad 250$ vehicles per hour Right Turns $\quad=\quad 100$ vehicles per hour

Problem: Determine if a right-turn lane is necessary.
Solution: $\quad$ To read the vertical axis, use $100-20=80$ vehicles per hour. The figure indicates that a right-turn lane is not necessary, unless other factors (e.g., high crash rate) indicate a lane is needed.

GUIDELINES FOR RIGHT-TURN LANES AT UNSIGNALIZED INTERSECTIONS ON TWO-LANE HIGHWAYS

Figure 9.5-A

| 2025 Build <br> Conditions | Major Road Volume (Direction <br> of Right Turn Ingress) | Right Turn <br> Volume | Speed along <br> Right Turn <br> Ingress | Symbol |
| :---: | :---: | :---: | :---: | :---: |
| AM Peak Hour | 541 | 4 | 45 | 0 |
| PM Peak Hour | 282 | 14 | 45 | $\square$ |

INTERSECTION: County Line Road \& Project Driveway 3
MOVEMENT: Northbound Left-Turn Lane
9.5-8 $\quad$ INTERSECTIONS $\quad$ March 2017


## Instructions:

1. The family of curves represents the percent of left turns in the advancing volume ( $V_{A}$ ). The designer should locate the curve for the actual percentage of left turns. When this is not an even increment of 5, the designer should estimate where the curve lies.
2. Read $V_{A}$ and $V_{O}$ into the chart and locate the intersection of the two volumes.
3. Note the location of the point in \#2 relative to the line in \#1. If the point is to the right of the line, then a left-turn lane is warranted. If the point is to the left of the line, then a leftturn lane is not warranted based on traffic volumes.

VOLUME GUIDELINES FOR LEFT-TURN LANES AT UNSIGNALIZED INTERSECTIONS ON TWO-LANE HIGHWAYS ( 45 mph )

Figure 9.5-F

| 2025 Build <br> Conditions | $\mathbf{V}_{\text {A }}$ | EBL | $\mathbf{V}_{\mathbf{O}}$ | V $_{\text {A }}$ LT \% | Symbol |
| :---: | :---: | :---: | :---: | :---: | :---: |
| AM Peak Hour | 225 | 37 | 541 | $16.4 \%$ | 0 |
| PM Peak Hour | 686 | 123 | 282 | $17.9 \%$ | $\square$ |

INTERSECTION: County Line Road \& Project Driveway 4
MOVEMENT: Eastbound Right-Turn Lane


Note: For highways with a design speed below 50 miles per hour with a DHV <300 and where right turns $>40$, an adjustment should be used. To read the vertical axis of the chart, subtract 20 from the actual number of right turns.

## Example

Design Speed $\quad=\quad 35$ miles per hour DHV $=\quad 250$ vehicles per hour Right Turns $\quad=\quad 100$ vehicles per hour

Problem: Determine if a right-turn lane is necessary.
Solution: $\quad$ To read the vertical axis, use $100-20=80$ vehicles per hour. The figure indicates that a right-turn lane is not necessary, unless other factors (e.g., high crash rate) indicate a lane is needed.

GUIDELINES FOR RIGHT-TURN LANES AT UNSIGNALIZED INTERSECTIONS ON TWO-LANE HIGHWAYS

Figure 9.5-A

| 2025 Build <br> Conditions | Major Road Volume (Direction <br> of Right Turn Ingress) | Right Turn <br> Volume | Speed along <br> Right Turn <br> Ingress | Symbol |
| :---: | :---: | :---: | :---: | :---: |
| AM Peak Hour | 454 | 3 | 45 | 0 |
| PM Peak Hour | 242 | 8 | 45 | $\square$ |

INTERSECTION: County Line Road \& Project Driveway 4
MOVEMENT: Westbound Left-Turn Lane
9.5-8 INTERSECTIONS March 2017


Instructions:

1. The family of curves represents the percent of left turns in the advancing volume $\left(V_{A}\right)$. The designer should locate the curve for the actual percentage of left turns. When this is not an even increment of 5, the designer should estimate where the curve lies.
2. Read $V_{A}$ and $V_{O}$ into the chart and locate the intersection of the two volumes.
3. Note the location of the point in \#2 relative to the line in \#1. If the point is to the right of the line, then a left-turn lane is warranted. If the point is to the left of the line, then a leftturn lane is not warranted based on traffic volumes.

VOLUME GUIDELINES FOR LEFT-TURN LANES AT UNSIGNALIZED INTERSECTIONS ON TWO-LANE HIGHWAYS ( 45 mph )

Figure 9.5-F

| 2025 Build <br> Conditions | $\mathbf{V}_{\mathrm{A}}$ | EBL | $\mathbf{V}_{\mathbf{O}}$ | $\mathbf{V}_{\mathrm{A}}$ LT \% | Symbol |
| :---: | :---: | :---: | :---: | :---: | :---: |
| AM Peak Hour | 190 | 12 | 454 | $6.3 \%$ | 0 |
| PM Peak Hour | 479 | 41 | 242 | $8.6 \%$ | $\square$ |

INTERSECTION: County Line Road \& Project Driveway 5
MOVEMENT: Eastbound Right-Turn Lane


Note: For highways with a design speed below 50 miles per hour with a DHV $<300$ and where right turns $>40$, an adjustment should be used. To read the vertical axis of the chart, subtract 20 from the actual number of right turns.

## Example

Design Speed $\quad=\quad 35$ miles per hour DHV $\quad=\quad 250$ vehicles per hour Right Turns $\quad=\quad 100$ vehicles per hour

Problem: Determine if a right-turn lane is necessary.
Solution: $\quad$ To read the vertical axis, use $100-20=80$ vehicles per hour. The figure indicates that a right-turn lane is not necessary, unless other factors (e.g., high crash rate) indicate a lane is needed.

GUIDELINES FOR RIGHT-TURN LANES AT UNSIGNALIZED INTERSECTIONS ON TWO-LANE HIGHWAYS

Figure 9.5-A

| 2025 Build <br> Conditions | Major Road Volume (Direction <br> of Right Turn Ingress) | Right Turn <br> Volume | Speed along <br> Right Turn <br> Ingress | Symbol |
| :---: | :---: | :---: | :---: | :---: |
| AM Peak Hour | 321 | 3 | 45 | 0 |
| PM Peak Hour | 179 | 8 | 45 | $\square$ |

INTERSECTION: County Line Road \& Project Driveway 5
MOVEMENT: Westbound Left-Turn Lane
9.5-8 INTERSECTIONS March 2017


## Instructions:

1. The family of curves represents the percent of left turns in the advancing volume $\left(V_{A}\right)$. The designer should locate the curve for the actual percentage of left turns. When this is not an even increment of 5, the designer should estimate where the curve lies.
2. Read $V_{A}$ and $V_{O}$ into the chart and locate the intersection of the two volumes.
3. Note the location of the point in \#2 relative to the line in \#1. If the point is to the right of the line, then a left-turn lane is warranted. If the point is to the left of the line, then a leftturn lane is not warranted based on traffic volumes.

VOLUME GUIDELINES FOR LEFT-TURN LANES AT UNSIGNALIZED INTERSECTIONS ON TWO-LANE HIGHWAYS ( 45 mph )

Figure 9.5-F

| 2025 Build <br> Conditions | $\mathbf{V}_{\mathrm{A}}$ | EBL | $\mathbf{V}_{\mathbf{O}}$ | $\mathbf{V}_{\mathbf{A}}$ LT \% | Symbol |
| :---: | :---: | :---: | :---: | :---: | :---: |
| AM Peak Hour | 159 | 4 | 321 | $3 \%$ | 0 |
| PM Peak Hour | 313 | 14 | 179 | $4 \%$ | $\square$ |

